

TPS631010 and TPS631011 1.5-A Output Current, Buck-Boost Converters in Small Wafer Chip Scale Package

1 Features

- 1.6-V to 5.5-V input voltage range
 - Device input voltage > 1.65 V for start-up
- 1.2-V to 5.5-V output voltage range (adjustable)
- High output current capability, 3-A peak switch current
 - 2-A output current for $V_{IN} \geq 3\text{ V}$, $V_{OUT} = 3.3\text{ V}$
 - 1.5-A output current for $V_{IN} \geq 2.7\text{ V}$, $V_{OUT} = 3.3\text{ V}$
- Active output discharge (TPS631011 only)
- High efficiency over the entire load range
 - 8- μA typical quiescent current
 - Automatic power save mode and forced PWM mode configurable
- Peak current buck-boost mode architecture
 - Seamless mode transition
 - Forward and reverse current operation
 - Start-up into pre-biased outputs
 - Fixed-frequency operation with 2-MHz switching
- Safety and robust operation features
 - Overcurrent protection and short-circuit protection
 - Integrated soft start with active ramp adoption
 - Overtemperature protection and overvoltage protection
 - True shutdown function with load disconnect
 - Forward and backward current limit
- Small solution size
 - Small 1- μH inductor
 - 1.803-mm \times 0.905-mm in WCSP
- Create a custom design using the TPS631010 and TPS631011 with the [WEBENCH® Power Designer](#)

2 Applications

- [TWS](#)
- System pre-regulator ([smartphone](#), [tablet](#), [terminal](#), [telematics](#))
- Point-of-load regulation (wired sensor, [port/cable adapter](#), and [dongle](#))
- Fingerprint, camera sensors ([electronic smart lock](#), [IP network camera](#))
- Voltage stabilizer (datacom, [optical modules](#), [cooling/heating](#))

3 Description

The TPS631010 and TPS631011 are constant frequency peak current mode control buck-boost converters in tiny wafer chip scale package. They have a 3-A peak current limit (typical) and 1.6-V to 5.5-V input voltage range, and provide a power supply solution for system pre-regulators and voltage stabilizers.

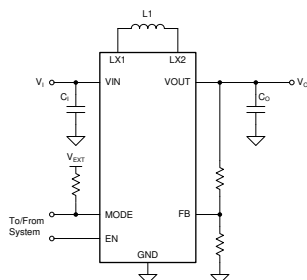
Depending on the input voltage, the TPS631010 and TPS631011 automatically operate in boost, buck, or in 3-cycle buck-boost mode when the input voltage is approximately equal to the output voltage. The transitions between modes happen at a defined duty cycle and avoid unwanted toggling within the modes to reduce output voltage ripple. 8- μA quiescent current and power save mode power enable the highest efficiency for light to no-load conditions.

The devices offer a very small solution size in WCSP.

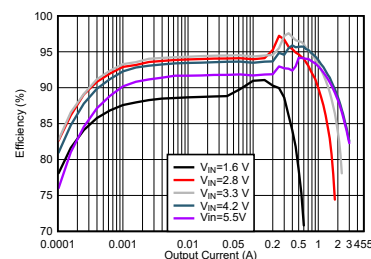
Package Information

Part Number	Package ⁽¹⁾	Body Size (NOM)
TPS631010	WCSP	1.803 mm \times 0.905 mm
TPS631011 ⁽²⁾		

- (1) For all available packages, see the orderable addendum at the end of the data sheet.
- (2) Preview information (not Production Data).



Typical Application



Efficiency Target vs Output Current ($V_{OUT} = 3.3\text{ V}$)



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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	REVISION	NOTES
December 2022	*	Advance Information

5 Device Comparison Table

PART NUMBER	Output Discharge
TPS631010	No
TPS631011 ⁽¹⁾	YES

(1) Product Preview. Contact TI factory for more information.

6 Pin Configuration and Functions

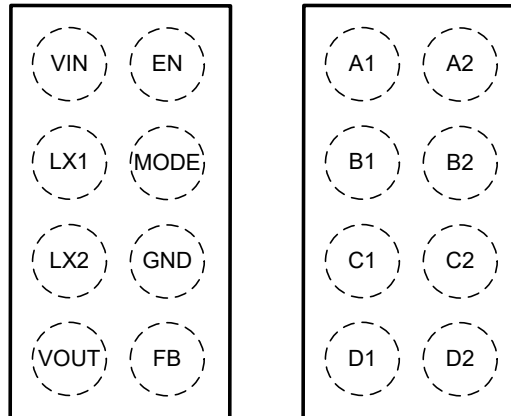


Figure 6-1. 8-Pin YBG WCSP Package (Top View)

Table 6-1. Pin Functions

PIN		I/O ⁽¹⁾	DESCRIPTION
NAME	NO.		
VIN	A1	PWR	Supply input voltage
EN	A2	I	Device enable. Set High to enable and Low to disable. It must not be left floating.
LX1	B1	PWR	Inductor switching node of the buck stage
MODE	B2	I	PFM/PWM selection. Set Low for power save mode, set High for forced PWM. It must not be left floating.
LX2	C1	PWR	Inductor switching node of the boost stage
GND	C2	PWR	Power ground
VOUT	D1	PWR	Power stage output
FB	D2	I	Voltage feedback. Sensing pin

(1) PWR = power, I = input

7 Specifications

7.1 Absolute Maximum Ratings

over operating junction temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
V _I	Input voltage (VIN, LX1, LX2, VOUT, EN, FB, MODE) ⁽²⁾	-0.3	6.0	V
	Input voltage for less than 10 ns (LX1, LX2) ⁽²⁾	-0.3	7	V
T _J	Operating junction temperature	-40	150	°C
T _{stg}	Storage temperature	-65	150	°C

- Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- All voltage values are with respect to network ground terminal, unless otherwise noted.

7.2 ESD Rating

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±1000	V
		Charged-device model (CDM), per JEDEC specification JS-002 ⁽²⁾	± 500	

- JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating junction temperature (unless otherwise noted)

			MIN	NOM	MAX	UNIT
V _I	Supply voltage		1.6		5.5	V
V _O	Output voltage		1.2		5.5	V
C _I	Effective Input capacitance	V _I = 1.6 V to 5.5 V	4.2			μF
C _O	Effective Output capacitance	1.2 V ≤ V _O ≤ 3.6 V, nominal value at V _O = 3.3 V	10.4	16.9	330	μF
		3.6 V < V _O ≤ 5.5 V, nominal value at V _O = 5 V	7.95	10.6	330	μF
L	Effective Inductance		0.7	1	1.3	μH
T _J	Operating junction temperature range		-40		125	°C

7.4 Thermal Information

over operating free-air temperature range (unless otherwise noted)

THERMAL METRIC		TPS631010	TPS631011	UNIT
		YBG(WCSP)		
		8		
R _{θJA}	Junction-to-ambient thermal resistance	84		°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	0.7		°C/W
R _{θJB}	Junction-to-board thermal resistance	43.9		°C/W
Ψ _{JT}	Junction-to-top characterization parameter	2.9		°C/W
Ψ _{JB}	Junction-to-board characterization parameter	43.7		°C/W
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	N/A		°C/W

7.5 Electrical Characteristics

Over operating junction temperature range and recommended supply voltage range (unless otherwise noted). Typical values are at $V_I = 3.8\text{ V}$, $V_O = 3.3\text{ V}$ and $T_J = 25^\circ\text{C}$ (unless otherwise noted).

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT	
SUPPLY								
I_{SD}	Shutdown current into VIN	$V_I = 3.8\text{ V}$, $V_{(EN)} = 0\text{ V}$ $T_J = 25^\circ\text{C}$			0.5	0.9	μA	
I_Q	Quiescent current into VIN	$V_I = 2.2\text{ V}$, $V_O = 3.3\text{ V}$, $V_{(EN)} = 2.2\text{ V}$, no switching			0.15	6.1	μA	
I_Q	Quiescent current into VOUT	$V_I = 2.2\text{ V}$, $V_O = 3.3\text{ V}$, $V_{(EN)} = 2.2\text{ V}$, no switching			8		μA	
V_{IT+}	Positive-going UVLO threshold voltage			1.5	1.55	1.599	V	
V_{IT-}	Negative-going UVLO threshold voltage	During start-up		1.4	1.45	1.499	V	
V_{hys}	UVLO threshold voltage hysteresis			99			mV	
$V_{I(POR)T+}$	Positive-going POR threshold voltage	maximum of V_I or V_O		1.25	1.45	1.65	V	
$V_{I(POR)T-}$	Negative-going POR threshold voltage			1.22	1.43	1.6	V	
I/O SIGNALS								
V_{T+}	Positive-going threshold voltage	EN, MODE		0.77	0.98	1.2	V	
V_{T-}	Negative-going threshold voltage	EN, MODE		0.5	0.66	0.76	V	
V_{hys}	Hysteresis voltage	EN, MODE			300		mV	
I_{IH}	High-level input current	(EN, MODE)	$V_{(EN)} = V_{(MODE)} = 1.5\text{ V}$, no pullup resistor		± 0.01	± 0.25	μA	
I_{IL}	Low-level input current	(EN, MODE)	$V_{(EN)} = V_{(MODE)} = 0\text{ V}$,		± 0.01	± 0.1	μA	
	Input bias current	(EN, MODE)	$V_{(EN)} = 5.5\text{ V}$		± 0.01	± 0.3	μA	
POWER SWITCH								
$r_{DS(on)}$	On-state resistance	Q1	$V_I = 3.8\text{ V}$, $V_O = 3.3\text{ V}$, test current = 0.2 A		45		m Ω	
		Q2			50		m Ω	
		Q3			50		m Ω	
		Q4			85		m Ω	
CURRENT LIMIT								
$I_{L(PEAK)}$	Switch peak current limit ⁽¹⁾	Q1	$V_O = 3.3\text{ V}$	Output sourcing current	2.6	3	3.35	A
				Output sinking current, $V_I = 3.3\text{ V}$	-0.7	-0.55	-0.45	A
	PFM mode entry threshold (peak) current ⁽¹⁾		I_O falling		145		mA	
OUTPUT								
I_{DIS}	TPS631011 Output discharge current	EN = LOW, $V_I = 2.2\text{ V}$ $V_O = 3.3\text{ V}$			-67		mA	
CONTROL[FEEDBACK PIN]								
V_{FB}	Reference voltage on feedback pin			495	500	505	mV	
PROTECTION FEATURES								
$V_{T+(OVP)}$	Positive-going OVP threshold voltage			5.55	5.75	5.95	V	
$V_{T+(IVP)}$	Positive-going IVP threshold voltage			5.55	5.75	5.95	V	
TIMING PARAMETERS								
$t_{d(EN)}$	Delay between a rising edge on the EN pin and the start of the output voltage ramp				0.87	1.5	ms	
$t_{d(ramp)}$	Soft-start ramp time			6.42	7.55	8.68	ms	
f_{SW}	Switching frequency			1.8	2	2.2	MHz	

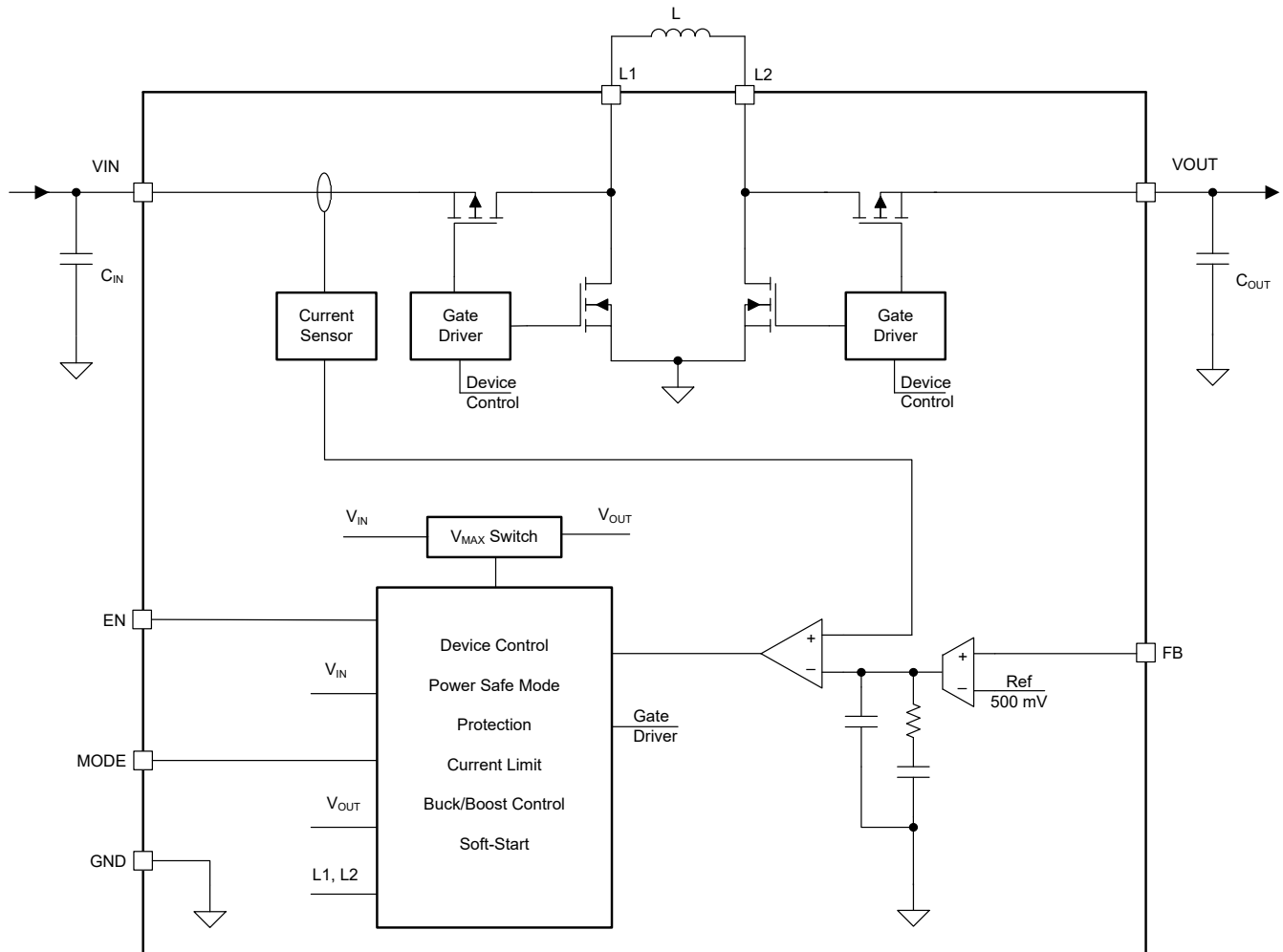
(1) Current limit production test are performed under DC conditions. The current limit in operation is somewhat higher and depending on propagation delay and the applied external components

8 Detailed Description

8.1 Overview

The TPS631010 and TPS631011 are a constant frequency peak current mode control buck-boost converters. The converters use a fixed-frequency topology with approximately 2-MHz switching frequency. The modulation scheme has three clearly defined operation modes where the converters enter with defined thresholds over the full operation range of V_{IN} and V_{OUT} . The maximum output current is determined by the Q1 peak current limit, which is typically 3 A.

8.2 Functional Block Diagram



8.3 Feature Description

8.3.1 Undervoltage Lockout (UVLO)

The input voltage of the VIN pin is continuously monitored if the device is not in shutdown mode. UVLO only stops or starts the converter operation. The UVLO does not impact the core logic of the device. UVLO avoids a brownout of the device during device operation. In case the supply voltage on the VIN pin is lower than the negative-going threshold of UVLO, the converter stops its operation. To avoid a false disturbance of the power conversion, the UVLO falling threshold logic signal is digitally de-glitched.

If the supply voltage on the VIN pin recovers to be higher than the UVLO rising threshold, the converter returns to operation. In this case, the soft-start procedure restarts faster than under start-up without a pre-biased output.

8.3.2 Enable and Soft Start

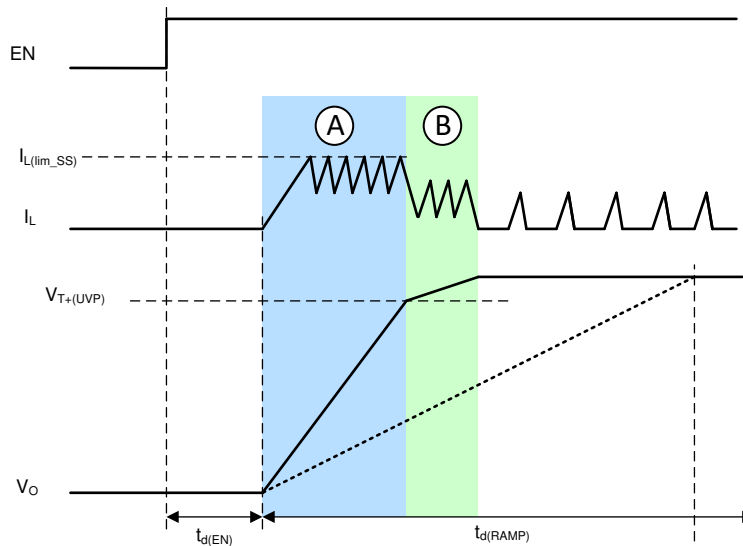


Figure 8-1. Typical Soft-Start Behavior

When the input voltage is above the UVLO rising threshold and the EN pin is pulled to a voltage above 1.2 V, the TPS631010 and TPS631011 are enabled and starts up after a short delay time, $t_{d(EN)}$.

The devices have an inductor peak current clamp to limit the inrush current during start-up. When the minimum current clamp ($I_{L(lim_SS)}$) is lower than the current that is necessary to follow the voltage ramp, the current automatically increases to follow the voltage ramp. The minimum current limit ensures as fast as possible soft start if the capacitance is chosen lower than what the ramp time $t_{d(RAMP)}$ was selected for.

In a typical start-up case as shown in [Figure 8-1](#) (low output load, typical output capacitance), the minimum current clamp limits the inrush current and charges the output capacitor. The output voltage then rises faster than the reference voltage ramp (see phase A in [Figure 8-1](#)). To avoid an output overshoot, the current clamp is deactivated when the output is close to the target voltage and follows the reference voltage ramp slew value given by the voltage ramp, which is finishing the start up (see phase B in [Figure 8-1](#)). The transition from the minimum current clamp operation is sensed by using the threshold $V_{T+(UVP)}$. After phase B, the output voltage is well regulated to the nominal target voltage. The current waveform depends on the output load and operation mode.

8.3.3 Adjustable Output Voltage

The output voltage is set by an external resistor divider. The resistor divider must be connected between VOUT, FB, and GND. The feedback voltage is given by V_{FB} . The low-side resistor R2 (between FB and GND) must not exceed 100 k Ω . The high-side resistor R1 (between FB and VOUT) is calculated by [Equation 1](#).

$$R1 = R2 \times (V_{OUT} / V_{FB} - 1) \quad (1)$$

The typical V_{FB} voltage is 0.5 V.

8.3.4 Mode Selection (PFM/FPWM)

The mode pin is a digital input to enable PFM/FPWM.

When the MODE pin is connected to logic low, the device works in auto PFM mode. The device features a power save mode to maintain the highest efficiency over the full operating output current range. PFM automatically changes the converter operation from CCM to pulse frequency modulation.

When the MODE pin is connected to logic high, the device works in forced PWM mode, regardless of the output current, to achieve minimum output ripple.

8.3.5 Output Discharge

TPS631011 provides an active pull down current(67mA typ) to quickly discharge output when the EN is logic low. With this function, the VOUT is connected to ground through internal circuitry, preventing the output from “floating” or entering into an undetermined state. The output discharge function makes the power on and off sequencing smooth. Pay attention to the output discharge function if use this device in applications such as power multiplexing, because the output discharge circuitry creates a constant current path between the multiplexer output and the ground.

8.3.6 Reverse Current Operation

The device can support reverse current operation (the current flows from VOUT pin to VIN pin). If the output feedback voltage on the FB pin is higher than the reference voltage, the converter regulation forces a current into the input capacitor. The reverse current operation is independent of the V_{IN} voltage or V_{OUT} voltage ratio, hence it is possible on all device operation modes boost, buck, or buck-boost.

8.3.7 Protection Features

The following sections describe the protection features of the device.

8.3.7.1 Input Overvoltage Protection

The TPS631010 and TPS631011 have input overvoltage protection which avoids any damage to the device in case the current flows from the output to the input and the input source cannot sink current (for example, a diode in the supply path).

If forced PWM mode is active, the current can go negative until it reaches the sink current limit. Once the input voltage threshold, $V_{T+(IVP)}$, is reached on the VIN pin, the protection disables forced PWM mode and only allows current to flow from VIN to VOUT. After the input voltage drops under the input voltage protection threshold, forced PWM mode can be activated again.

8.3.7.2 Output Overvoltage Protection

The devices have the output overvoltage protection which avoids any damage to the device in case the external feedback pin is not working properly.

If the output voltage threshold $V_{T+(OVP)}$ is reach on the VOUT pin, the protection disables converter power stage and enter a high impedance at the switch nodes.

8.3.7.3 Short Circuit Protection

The device features peak current limit performance at short circuit protection. [Figure 8-2](#) shows a typical device behavior of an short/overload event of the short circuit protection.

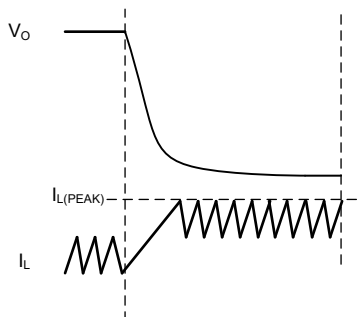


Figure 8-2. Typical Device Behavior During Short Circuit Protection

8.3.7.4 Thermal Shutdown

To avoid thermal damage of the device, the temperature of the die is monitored. The device stops operation once the sensed temperature rises over the thermal threshold. After the temperature drops below the thermal shutdown hysteresis, the converter returns to normal operation.

8.4 Device Functional Modes

The device has two functional modes: off and on. The device enters the on mode when the voltage on the VIN pin is higher than the UVLO threshold and a high logic level is applied to the EN pin. The device enters the off mode when the voltage on the VIN pin is lower than the UVLO threshold or a low logic level is applied to the EN pin.

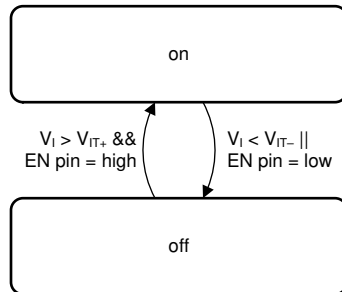


Figure 8-3. Device Functional Modes

9 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

9.1 Application Information

The TPS631010 and TPS631011 are a high-efficiency, low-quiescent current, buck-boost converters. The device is suitable for applications needing a regulated output voltage from an input supply that can be higher or lower than the output voltage.

9.2 Typical Application

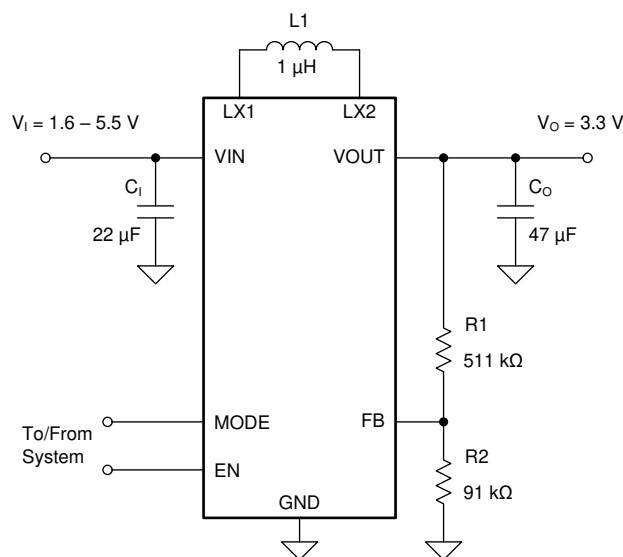


Figure 9-1. 3.3-V_{OUT} Typical Application

9.2.1 Design Requirements

The design parameters are listed in [Table 9-1](#).

Table 9-1. Design Parameters

PARAMETERS	VALUES
Input voltage	2.7 V to 4.3 V
Output voltage	3.3 V
Output current	1.5 A

9.2.2 Detailed Design Procedure

The first step is the selection of the output filter components. To simplify this process, [Recommended Operating Conditions](#) outlines minimum and maximum values for inductance and capacitance. Pay attention to the tolerance and derating when selecting nominal inductance and capacitance.

9.2.2.1 Custom Design with WEBENCH Tools

[Click here](#) to create a custom design using the TPS631010 and TPS631011 with the WEBENCH® Power Designer.

1. Start by entering your V_{IN}, V_{OUT} and I_{OUT} requirements.

2. Optimize your design for key parameters like efficiency, footprint or cost using the optimizer dial and compare this design with other possible solutions from Texas Instruments.
3. WEBENCH Power Designer provides you with a customized schematic along with a list of materials with real time pricing and component availability.
4. In most cases, you can:
 - Run electrical simulations to see important waveforms and circuit performance,
 - Run thermal simulations to understand the thermal performance of your board,
 - Export your customized schematic and layout into popular CAD formats,
 - Print PDF reports for the design, and share your design with colleagues.
5. Get more information about WEBENCH tools at www.ti.com/webench.

9.2.2.2 Inductor Selection

The inductor selection is affected by several parameters such as the following:

- Inductor ripple current
- Output voltage ripple
- Transition point into power save mode
- Efficiency

See [Table 9-2](#) for typical inductors.

For high efficiencies, the inductor with a low DC resistance is needed to minimize conduction losses. Especially at high-switching frequencies, the core material has a high impact on efficiency. When using small chip inductors, the efficiency is reduced mainly due to higher inductor core losses. Core losses need to be considered when selecting the appropriate inductor. The inductor value determines the inductor ripple current. The larger the inductor value, the smaller the inductor ripple current and the lower the conduction losses of the converter. Conversely, larger inductor values cause a slower load transient response. To avoid saturation of the inductor, the peak current for the inductor in steady state operation is calculated using [Equation 3](#). Only the equation that defines the switch current in boost mode is shown because this provides the highest value of current and represents the critical current value for selecting the right inductor.

$$\text{Duty Cycle Boost} \quad D = \frac{V_{\text{OUT}} - V_{\text{IN}}}{V_{\text{OUT}}} \quad (2)$$

$$I_{\text{PEAK}} = \frac{I_{\text{out}}}{\eta \times (1 - D)} + \frac{V_{\text{in}} \times D}{2 \times f \times L} \quad (3)$$

where:

- D = duty cycle in boost mode
- f = converter switching frequency (typical 2 MHz)
- L = inductor value
- η = estimated converter efficiency (use the number from the efficiency curves or 0.9 as an assumption)

Note

The calculation must be done for the minimum input voltage in boost mode.

Calculating the maximum inductor current using the actual operating conditions gives the minimum saturation current of the inductor needed. It is recommended to choose an inductor with a saturation current 20% higher than the value calculated using [Equation 3](#). Possible inductors are listed in [Table 9-2](#).

Table 9-2. List of Recommended Inductors

INDUCTOR VALUE [μ H]	SATURATION CURRENT [A]	DCR [m Ω]	PART NUMBER	MANUFACTURER ⁽¹⁾	SIZE (L \times W \times H mm)
1	4.3	42	DFE252012P-1R0M=P2	MuRata	2.5 \times 2.0 \times 1.2
1	4.2	43	HTEK20161T-1R0MSR	Cyntec	2.0 \times 1.6 \times 1.0
1	2.2	75	MAKK2016T1R0M ⁽²⁾	Taiyo Yuden	2.0 \times 1.6 \times 1.0
1	2.0	144	DFE18SAN1R0ME0 ⁽²⁾	Murata	1.6 \times 0.8 \times 0.8

- (1) See the [Third-Party Products Disclaimer](#).
(2) This inductor does not support full output current range.

9.2.2.3 Output Capacitor Selection

For the output capacitor, use small ceramic capacitors placed as close as possible to the VOUT and PGND pins of the IC. The recommended nominal output capacitor value is a single 47 μ F. If, for any reason, the application requires the use of large capacitors that cannot be placed close to the IC, use a smaller ceramic capacitor in parallel to the large capacitor, and place the small capacitor as close as possible to the VOUT and PGND pins of the IC.

It is important that the effective capacitance is given according to the recommended value in [Recommended Operating Conditions](#). In general, consider DC bias effects resulting in less effective capacitance. The choice of the output capacitance is mainly a tradeoff between size and transient behavior as higher capacitance reduces transient response over/undershoot and increases transient response time. Possible output capacitors are listed in [Table 9-3](#).

There is no upper limit for the output capacitance value.

Table 9-3. List of Recommended Capacitors

CAPACITOR VALUE [μ F]	VOLTAGE RATING [V]	ESR [m Ω]	PART NUMBER	MANUFACTURER ⁽¹⁾	SIZE (METRIC)
47	6.3	10	GRM219R60J476ME44	Murata	0805 (2012)
47	10	40	CL10A476MQ8QRN	Semco	0603 (1608)

- (1) See the [Third-Party Products Disclaimer](#).

9.2.2.4 Input Capacitor Selection

A 22- μ F input capacitor is recommended to improve line transient behavior of the regulator and EMI behavior of the total power supply circuit. An X5R or X7R ceramic capacitor placed as close as possible to the VIN and PGND pins of the IC is recommended. This capacitance can be increased without limit. If the input supply is located more than a few inches from the converter, additional bulk capacitance can be required in addition to the ceramic bypass capacitors. An electrolytic or tantalum capacitor with a value of 47 μ F is a typical choice.

Table 9-4. List of Recommended Capacitors

CAPACITOR VALUE [μ F]	VOLTAGE RATING [V]	ESR [m Ω]	PART NUMBER	MANUFACTURER ⁽¹⁾	SIZE (METRIC)
22	6.3	43	GRM187R61A226ME15	Murata	0603 (1608)
10	10	40	GRM188R61A106ME69	Murata	0603 (1608)

- (1) See the [Third-Party Products Disclaimer](#).

9.2.2.5 Setting the Output Voltage

The output voltage is set by an external resistor divider. The resistor divider must be connected between VOUT, FB, and GND. The feedback voltage is 500 mV nominal.

Keep the low-side resistor R2 (between FB and GND) below 100 k Ω . The high-side resistor (between FB and VOUT) R1 is calculated with [Equation 4](#).

$$R1 = R2 \times \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (4)$$

where

- $V_{FB} = 500 \text{ mV}$

Table 9-5. Resistor Selection For Typical Output Voltages

V_{OUT}	R1	R2
2.5 V	365K	91K
3.3 V	511K	91K
3.6 V	562K	91K
5 V	806K	91K

9.2.3 Application Curves

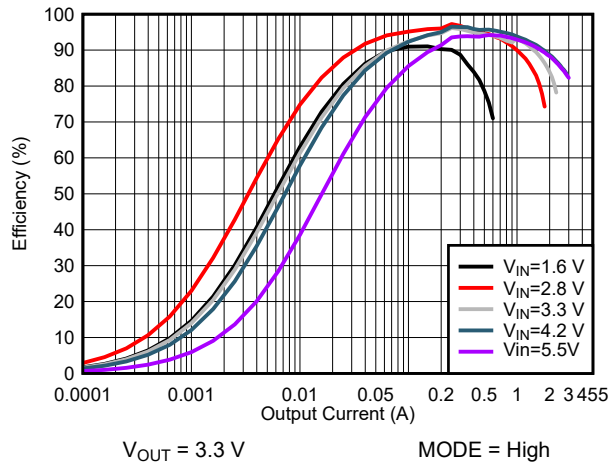


Figure 9-2. Efficiency vs Output Current (FPWM)

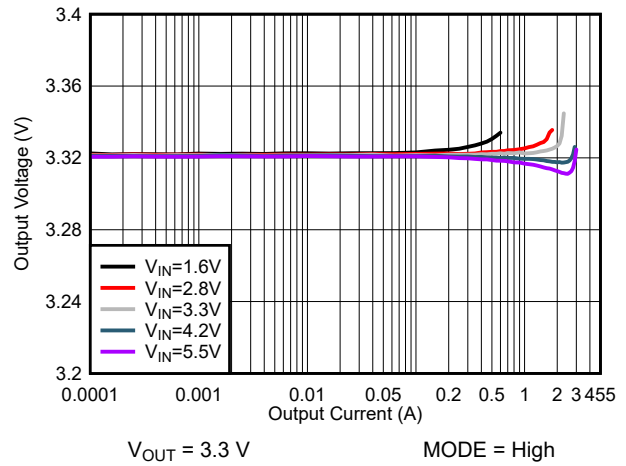


Figure 9-3. Load Regulation (FPWM)

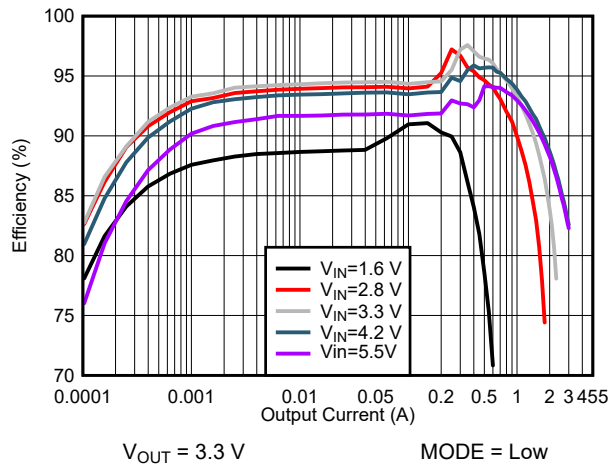


Figure 9-4. Efficiency vs Input Voltage (PFM)

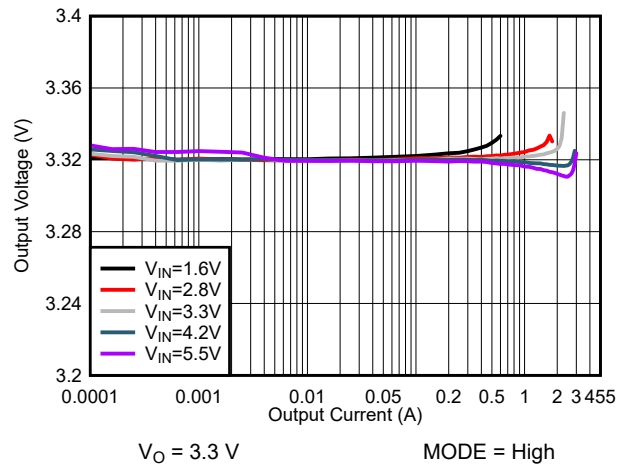


Figure 9-5. Load Regulation (PFM)

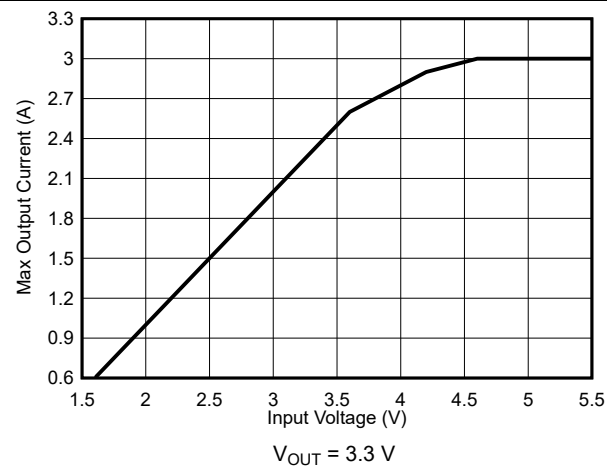


Figure 9-6. Typical Output Current Capability vs Input Voltage

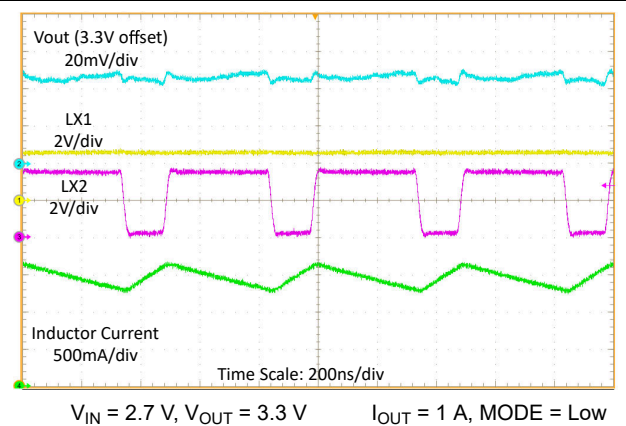
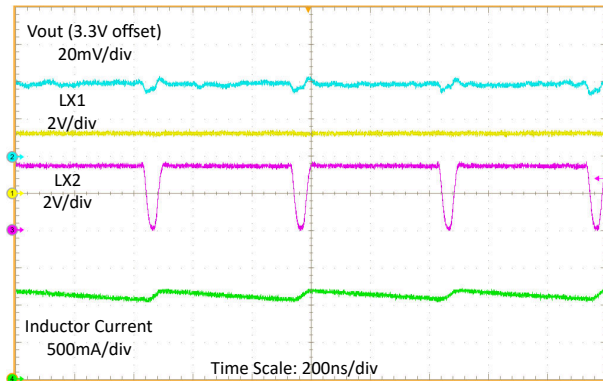
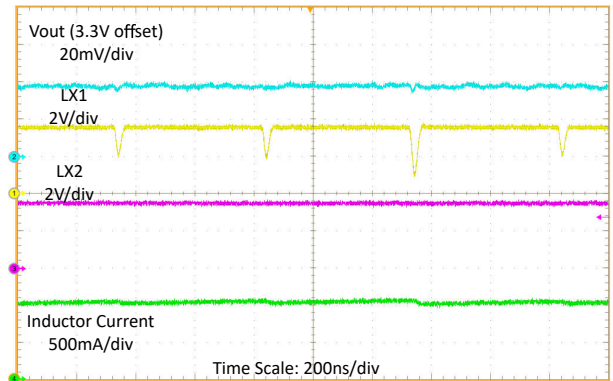


Figure 9-7. Switching Waveforms, Boost Operation with 1-A Load



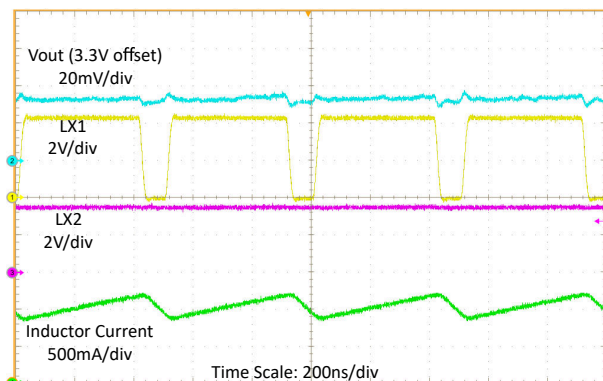
$V_{IN} = 3.3\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$, MODE = Low

Figure 9-8. Switching Waveforms with 1-A Load



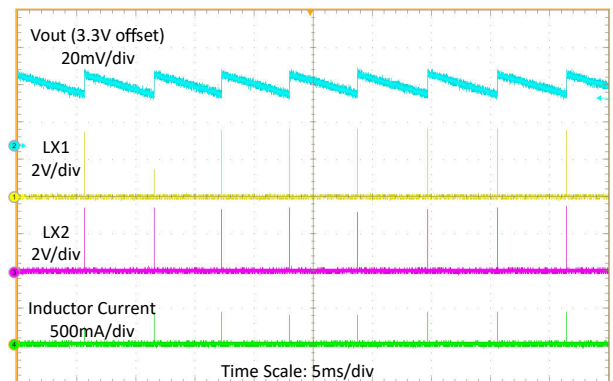
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$, MODE = Low

Figure 9-9. Switching Waveforms with 1-A Load



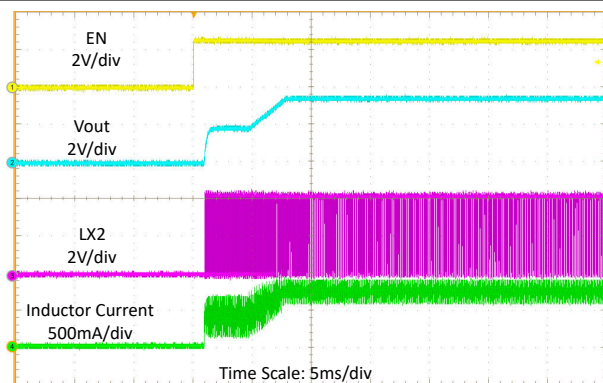
$V_{IN} = 4.3\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$, MODE = Low

Figure 9-10. Switching Waveforms, Buck Operation with 1-A Load



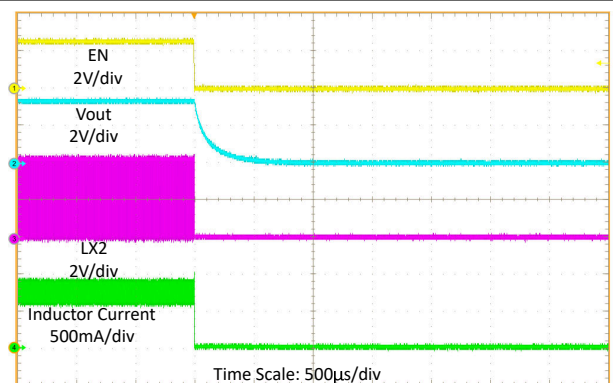
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ mA}$, MODE = Low

Figure 9-11. Switching Waveforms at 1-mA Load



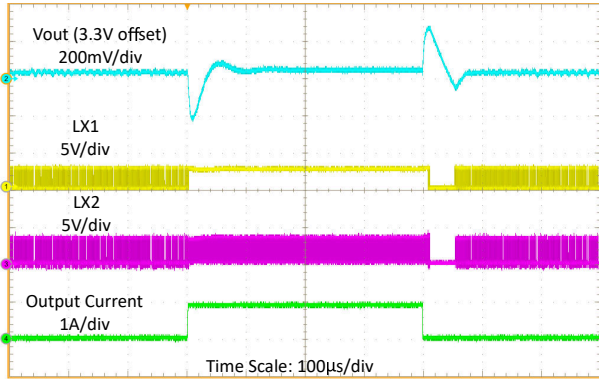
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $R_{load} = 4\ \Omega$, MODE = Low

Figure 9-12. Start-Up by EN



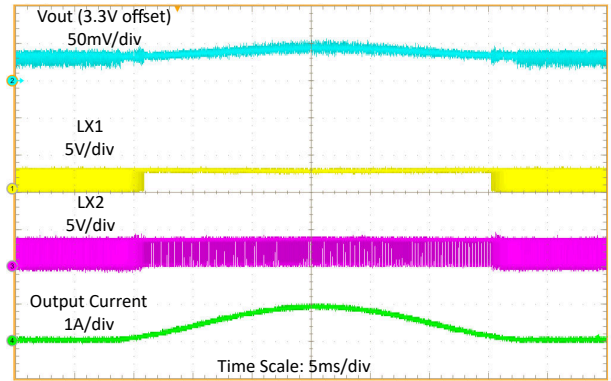
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $R_{load} = 4\ \Omega$, MODE = Low

Figure 9-13. Shutdown by EN



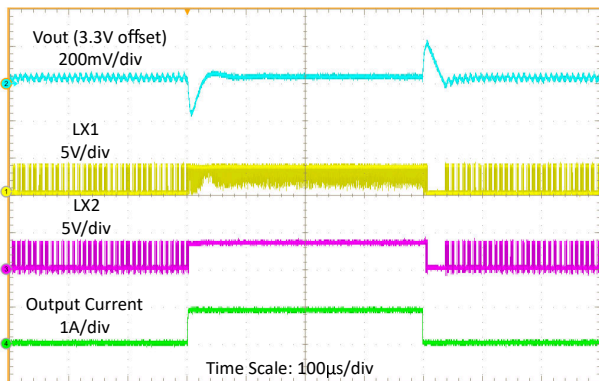
$V_{IN} = 2.7\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{ A}$ with $20\text{-}\mu\text{s}$ slew rate

Figure 9-14. Load Transient at 2.7-V Input Voltage



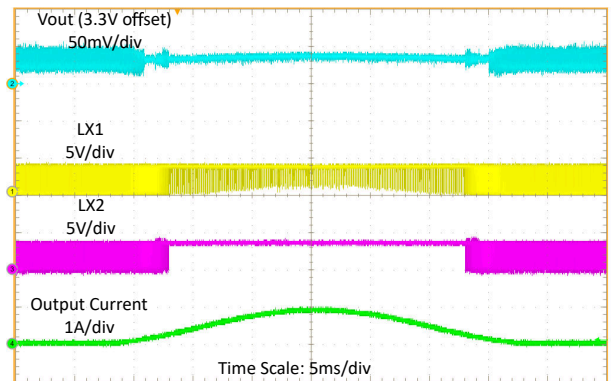
$V_{IN} = 2.7\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{-A sweep}$

Figure 9-15. Load Sweep at 2.7-V Input Voltage



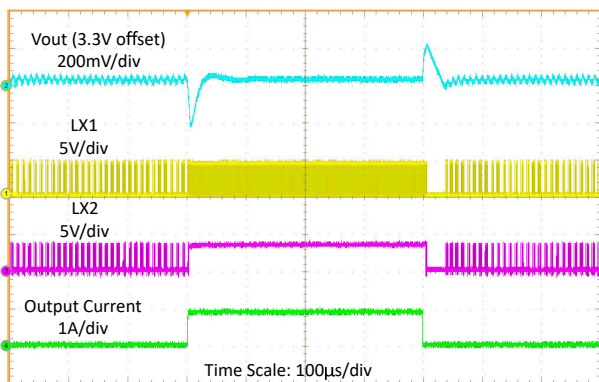
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{ A}$ with $20\text{-}\mu\text{s}$ slew rate

Figure 9-16. Load Transient at 3.6-V Input Voltage



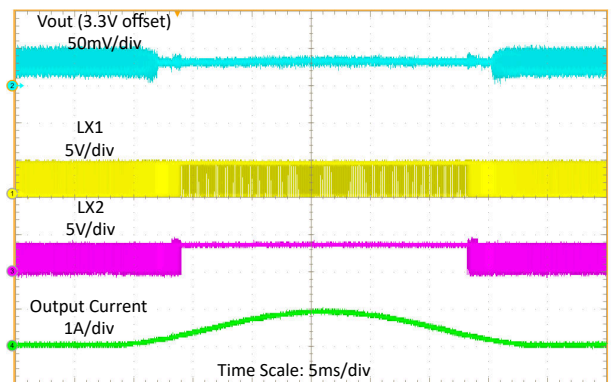
$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{-A sweep}$

Figure 9-17. Load Sweep at 3.6-V Input Voltage



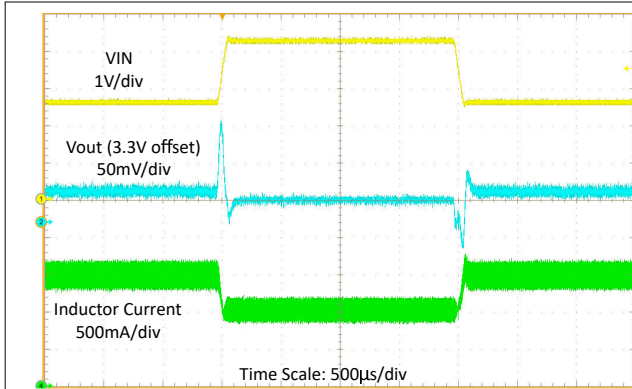
$V_{IN} = 4.3\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{ A}$ with $20\text{-}\mu\text{s}$ slew rate

Figure 9-18. Load Transient at 4.3-V Input Voltage



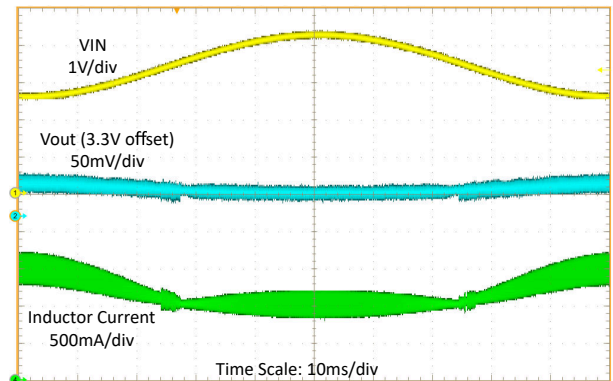
$V_{IN} = 4.3\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 100\text{ mA to }1\text{-A sweep}$

Figure 9-19. Load Sweep at 4.3-V Input Voltage



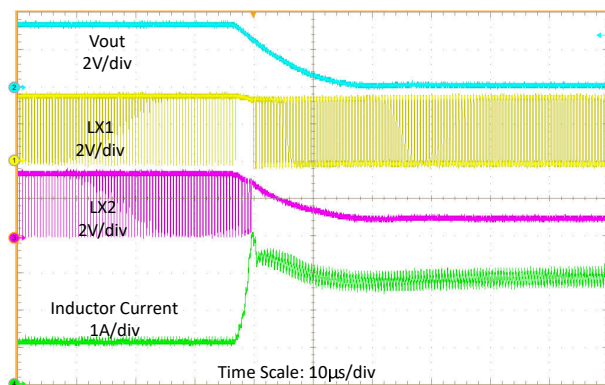
$V_{IN} = 2.7\text{ V to } 4.3\text{ V}$ with 20- μs slew rate, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$

Figure 9-20. Line Transient at 1-A Load Current



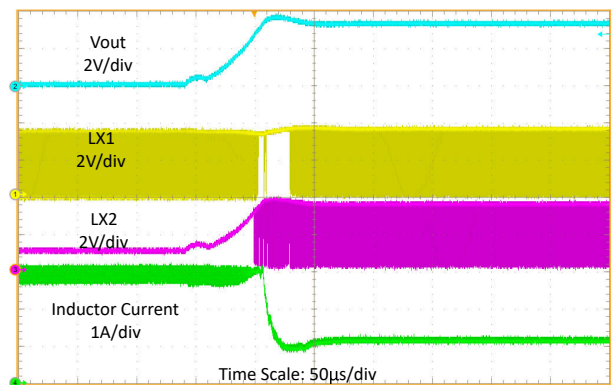
$V_{IN} = 2.7\text{-V to } 4.3\text{-V sweep}$, $I_{OUT} = 1\text{ A}$
 $V_{OUT} = 3.3\text{ V}$

Figure 9-21. Line Sweep at 1-A Load Current



$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$, FPWM

Figure 9-22. Output Short Protection (Entry)



$V_{IN} = 3.6\text{ V}$, $V_{OUT} = 3.3\text{ V}$ $I_{OUT} = 1\text{ A}$, FPWM

Figure 9-23. Output Short Protection (Recover)

Table 9-6. Components for Application Characteristic Curves for $V_{OUT} = 3.3\text{ V}$

REFERENCE	DESCRIPTION ⁽²⁾	PART NUMBER	MANUFACTURER ⁽¹⁾
U1	High Power Density 1.5 A Buck-Boost Converter	TPS631010 or TPS631011	Texas Instruments
L1	1.0 μH , 2.5 mm x 2.0 mm, 4.3 A, 42 m Ω	DFE252012P-1R0M=P2	MuRata
C1	22 μF , 0603, Ceramic Capacitor, $\pm 20\%$, 6.3 V	GRM187R61A226ME15	Murata
C2	47 μF , 0805, Ceramic Capacitor, $\pm 20\%$, 6.3 V	GRM219R60J476ME44	Murata
R1	511 k Ω , 0603 Resistor, 1%, 100 mW	Standard	Standard
R2	91 k Ω , 0603 Resistor, 1%, 100 mW	Standard	Standard

(1) See the [Third-Party Products Disclaimer](#).

(2) For other output voltages, refer to [Table 9-5](#) for resistor values.

9.3 Power Supply Recommendations

The TPS631010 and TPS631011 have no special requirements for its input power supply. The input power supply output current needs to be rated according to the supply voltage, output voltage, and output current.

9.4 Layout

9.4.1 Layout Guidelines

The PCB layout is an important step to maintain the high performance of the device.

- Place input and output capacitors as close as possible to the IC. Traces need to be kept short. Route wide and direct traces to the input and output capacitors results in low trace resistance and low parasitic inductance.
- The sense trace connected to FB is signal trace. Keep these traces away from L1 and L2 nodes.

9.4.2 Layout Example

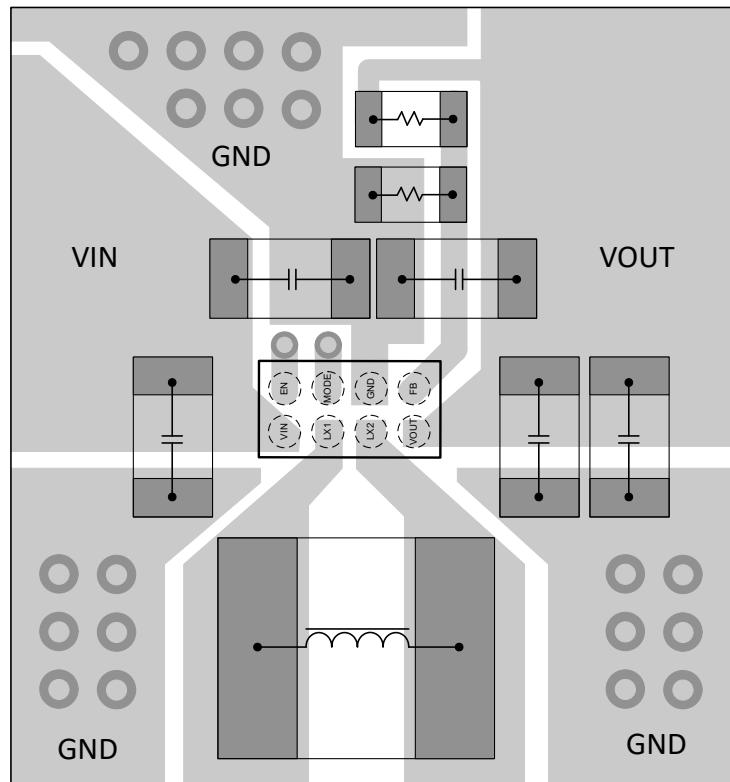


Figure 9-24. Layout Example

10 Device and Documentation Support

10.1 Device Support

10.1.1 Third-Party Products Disclaimer

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10.1.2 Development Support

10.1.2.1 Custom Design with WEBENCH Tools

[Click here](#) to create a custom design using the TPS631010 and TPS631011 with the WEBENCH® Power Designer.

1. Start by entering your V_{IN} , V_{OUT} and I_{OUT} requirements.
2. Optimize your design for key parameters like efficiency, footprint or cost using the optimizer dial and compare this design with other possible solutions from Texas Instruments.
3. WEBENCH Power Designer provides you with a customized schematic along with a list of materials with real time pricing and component availability.
4. In most cases, you can:
 - Run electrical simulations to see important waveforms and circuit performance,
 - Run thermal simulations to understand the thermal performance of your board,
 - Export your customized schematic and layout into popular CAD formats,
 - Print PDF reports for the design, and share your design with colleagues.
5. Get more information about WEBENCH tools at www.ti.com/webench.

10.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

10.3 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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10.4 Trademarks

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10.5 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

10.6 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS631010YBGR	ACTIVE	DSBGA	YBG	8	3000	RoHS & Green	SNAGCU	Level-1-260C-UNLIM	-40 to 125	1NS	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSELETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

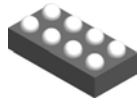
(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

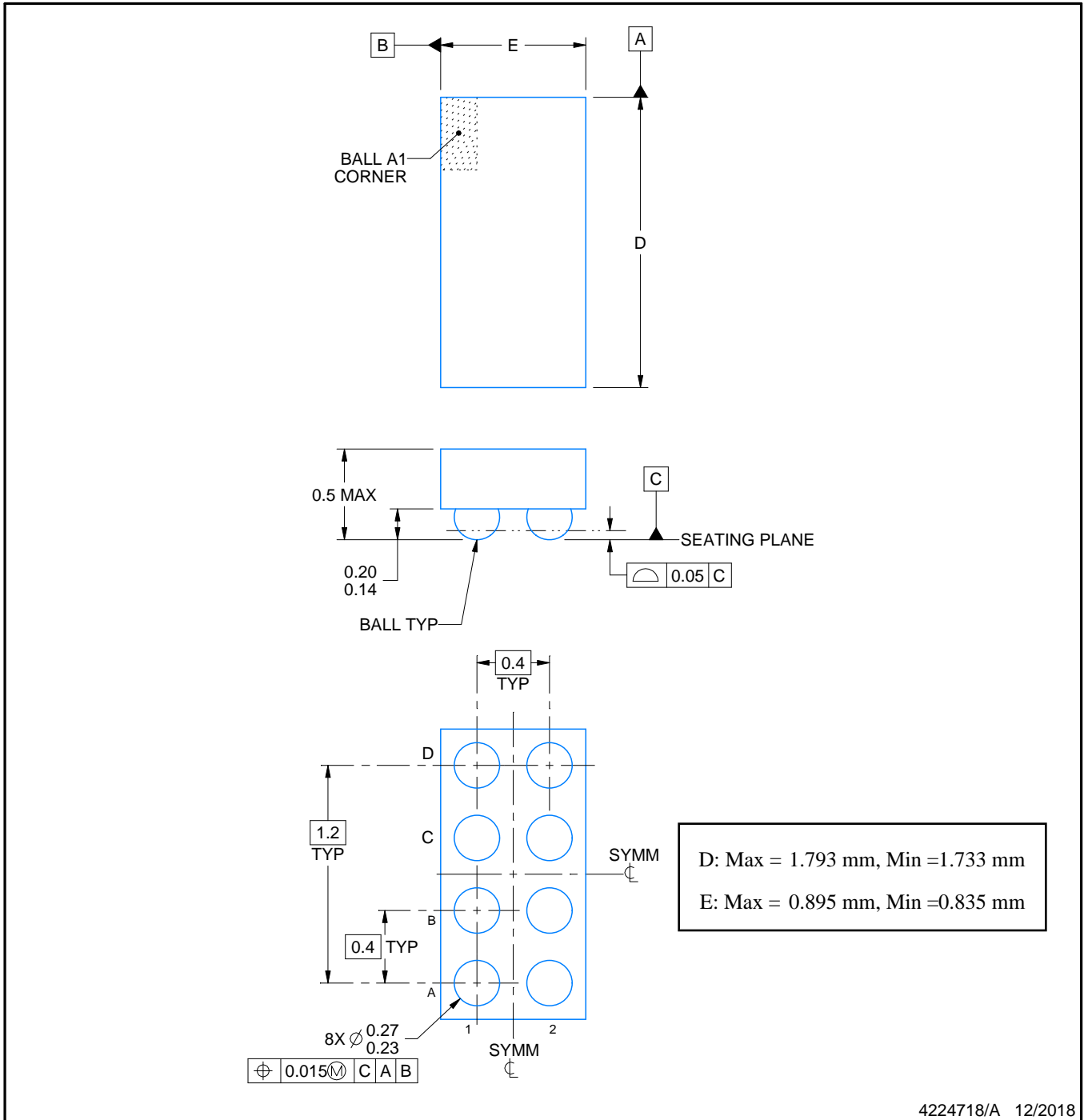
YBG0008



PACKAGE OUTLINE

DSBGA - 0.5 mm max height

DIE SIZE BALL GRID ARRAY



NOTES:

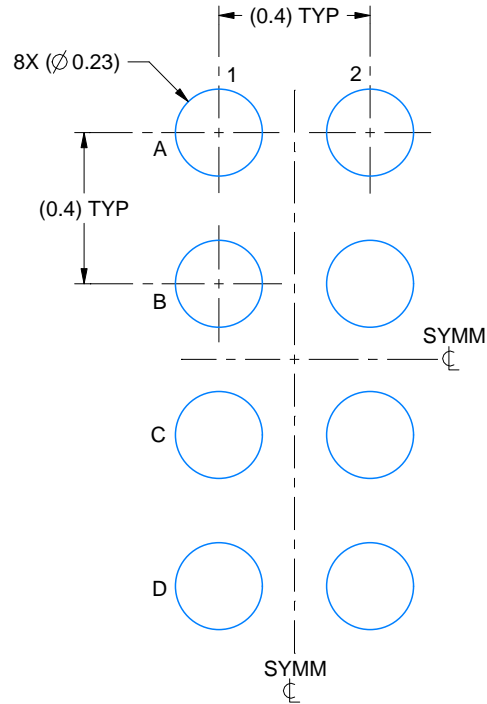
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.

EXAMPLE BOARD LAYOUT

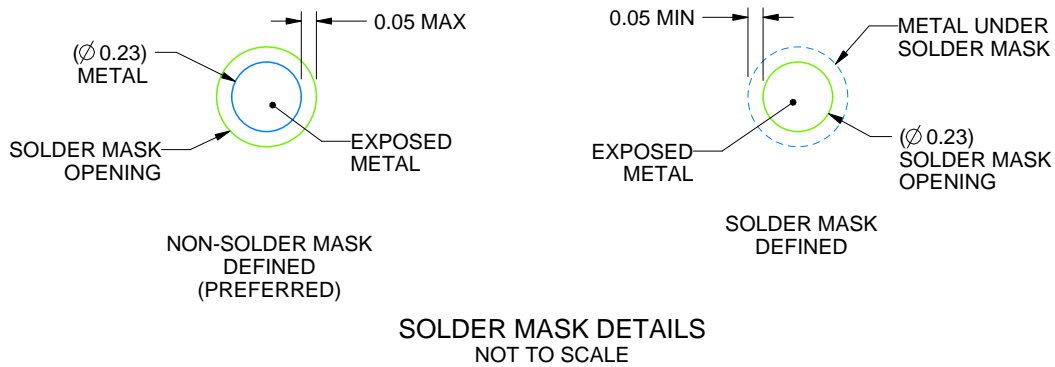
YBG0008

DSBGA - 0.5 mm max height

DIE SIZE BALL GRID ARRAY



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 50X



SOLDER MASK DETAILS
NOT TO SCALE

4224718/A 12/2018

NOTES: (continued)

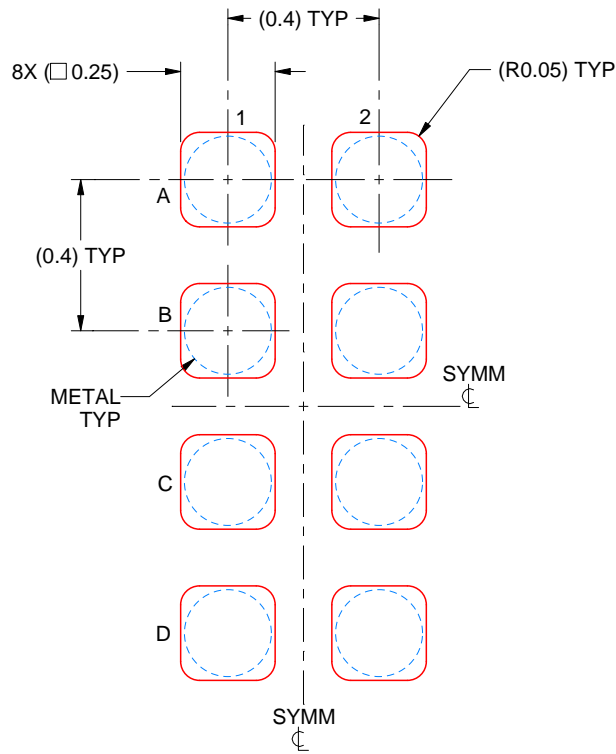
- Final dimensions may vary due to manufacturing tolerance considerations and also routing constraints. See Texas Instruments Literature No. SNVA009 (www.ti.com/lit/snva009).

EXAMPLE STENCIL DESIGN

YBG0008

DSBGA - 0.5 mm max height

DIE SIZE BALL GRID ARRAY



SOLDER PASTE EXAMPLE
BASED ON 0.1 mm THICK STENCIL
SCALE: 50X

4224718/A 12/2018

NOTES: (continued)

4. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release.

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