

Auxiliary Switch Diodes for Snubber SARS01, SARS02, SARS05, SARS10

Data Sheet

Description

The SARS⁽¹⁾ is an auxiliary switch diode especially designed for snubber circuits, which are used in the primary sides of flyback switched-mode power supplies.

Being capable of reducing the ringing voltage generated at power MOSFET turn-off, the SARS-incorporated snubber circuits allow better cross regulation of multiple outputs.

The SARS can also improve power supply efficiency by partially transferring such ringing voltage into the secondary side of a power supply unit.

Features

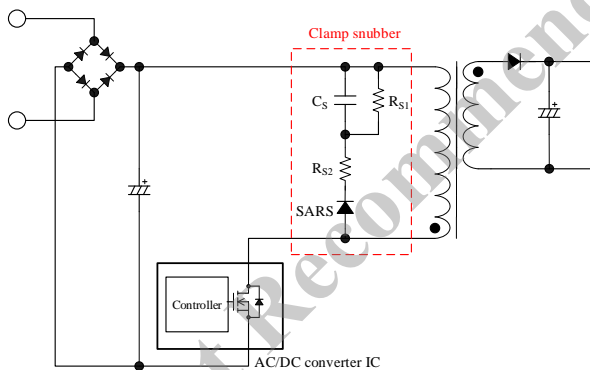
- Improves Cross Regulation
- Reduces Noise
- Improves Efficiency

Applications

For switched-mode power supplies (SMPS) with flyback topology such as:

- White Goods
- Adaptor
- Industrial Equipment

Typical Application



Package

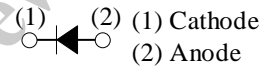
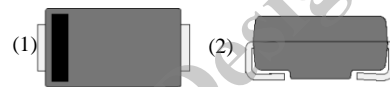
SARS01 (Axial ϕ 2.7 / ϕ 0.60)



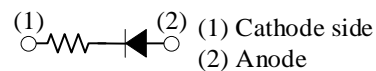
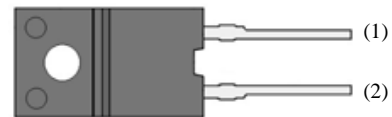
SARS02 (Axial ϕ 4 / ϕ 0.78)



SARS05 (SJP 4.5 mm \times 2.6 mm)



SARS10 (TO220F-2L)



Not to scale

Selection Guide

R_{S2}	Part Number	$I_{F(AV)}$	V_F (max.)	Power Supply Output Power, P_O^*
External Resistor	SARS01	1.2 A	0.92 V	up to 50 W
	SARS02	1.5 A	0.92 V	up to 100 W
	SARS05	1 A	1.05 V	up to 50 W
Built-in 22 Ω	SARS10	0.3 A	13 V	up to 300 W

* P_O represents a reference value for product selection. When using the product, you should monitor temperature rises during actual operation.

⁽¹⁾ The "SARS" represents any one of the SARSxx devices listed in this document.

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Not Recommended for New Designs

SARS01, SARS02, SARS05, SARS10

Absolute Maximum Ratings

Unless otherwise specified, $T_A = 25\text{ }^\circ\text{C}$, only the SARS10 incorporates a resistor ($22\ \Omega$).

Parameter	Symbol	Conditions	Rating	Unit	Remarks
Transient Peak Reverse Voltage	V_{RSM}		800	V	
Peak Repetitive Reverse Voltage	V_{RM}		800	V	
Average Forward Current ⁽²⁾	$I_{F(AV)}$		1.2	A	SARS01
			1.2		SARS02
			1.0		SARS05
			0.3		SARS10
Surge Forward Current	I_{FSM}	Half cycle sine wave, positive side, 10 ms, 1 shot	110	A	SARS01
			100		SARS02
			30		SARS05
		1 ms, square pulse, 1 shot	1.5		SARS10
I^2t Limiting Value	I^2t	$1\text{ ms} \leq t \leq 10\text{ ms}$	60.5	A^2s	SARS01
			50		SARS02
			4.5		SARS05
			—		SARS10
Junction Temperature	T_J		-40 to 150	$^\circ\text{C}$	SARS01/02/05
			-20 to 125		SARS10
Storage Temperature	T_{STG}		-40 to 150	$^\circ\text{C}$	SARS01/02/05
			-20 to 125		SARS10
Power Dissipation	P		3.0	W	SARS10

⁽²⁾ See the derating curves of each product.

SARS01, SARS02, SARS05, SARS10

Electrical Characteristics

Unless otherwise specified, $T_A = 25\text{ }^\circ\text{C}$, only the SARS10 incorporates a resistor ($22\text{ }\Omega$).

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit	Remarks
Forward Voltage Drop	V_F	$I_F = 1.2\text{ A}$	—	—	0.92	V	SARS01
		$I_F = 1.5\text{ A}$	—	—	0.92		SARS02
		$I_F = 1.0\text{ A}$	—	—	1.05		SARS05
		$I_F = 0.5\text{ A}$	—	—	13		SARS10
Reverse Leakage Current	I_R	$V_R = V_{RM}$	—	—	10	μA	SARS01
			—	—	10		SARS02
			—	—	5		SARS05
			—	—	10		SARS10
Reverse Leakage Current under High Temperature	$H \cdot I_R$	$V_R = V_{RM}$, $T_J = 100\text{ }^\circ\text{C}$	—	—	50	μA	SARS01/02/05
		$V_R = V_{RM}$, $T_J = 125\text{ }^\circ\text{C}$	—	—	100		SARS10
Reverse Recovery Time	t_{rr}	$I_F = I_{RP} = 100\text{ mA}$, $T_J = 25\text{ }^\circ\text{C}$, 90% recovery point	2	—	18	μs	SARS01
			2	—	18		SARS02
			2	—	19		SARS05
			1	—	9		SARS10
Thermal Resistance	$R_{th(J-L)}$	⁽³⁾	—	—	20	$^\circ\text{C/W}$	SARS01
			—	—	15		SARS02
			—	—	20		SARS05
	$R_{th(J-C)}$	⁽⁴⁾	—	—	15	$^\circ\text{C/W}$	SARS10

⁽³⁾ $R_{th(J-L)}$ is thermal resistance between junction and lead.

⁽⁴⁾ $R_{th(J-C)}$ is thermal resistance between junction and case.

SARS01 Rating and Characteristic Curves

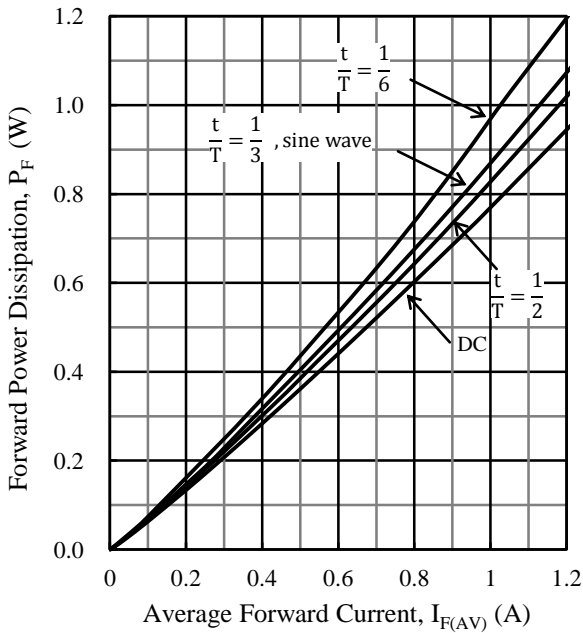


Figure 1. $I_{F(AV)}$ vs. P_F Power Dissipation Curves ($T_J = 150\text{ }^\circ\text{C}$)

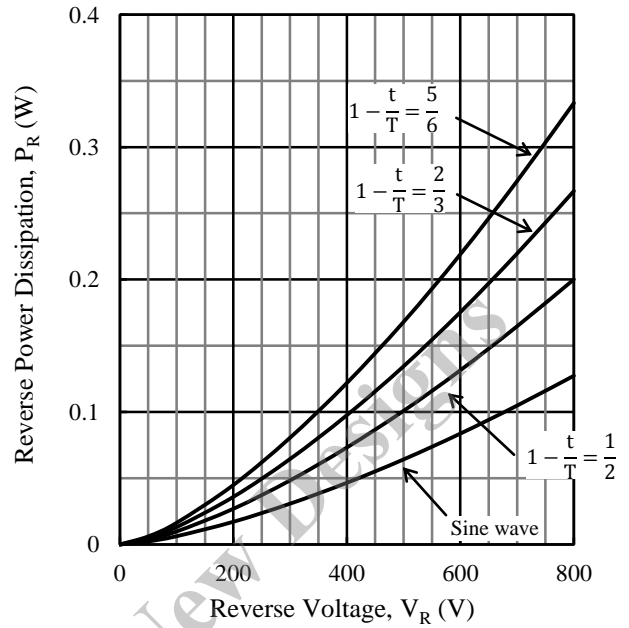


Figure 2. V_R vs. P_R Power Dissipation Curves ($T_J = 150\text{ }^\circ\text{C}$)

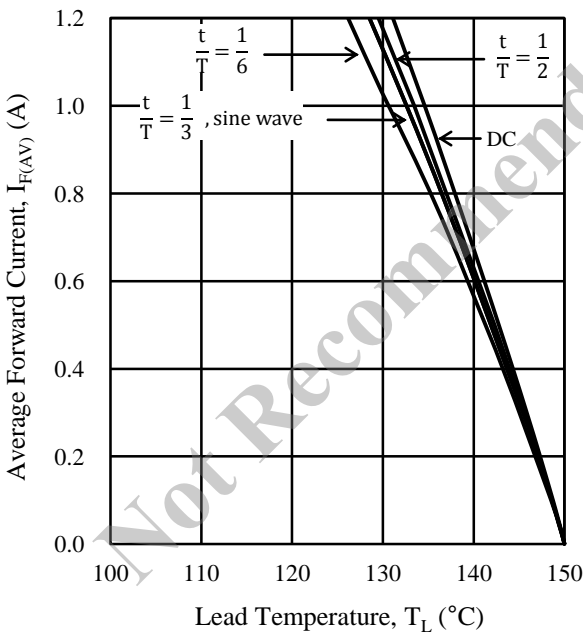


Figure 3. T_L vs. $I_{F(AV)}$ Derating Curves ($V_R = 0\text{ V}$, $T_J = 150\text{ }^\circ\text{C}$)

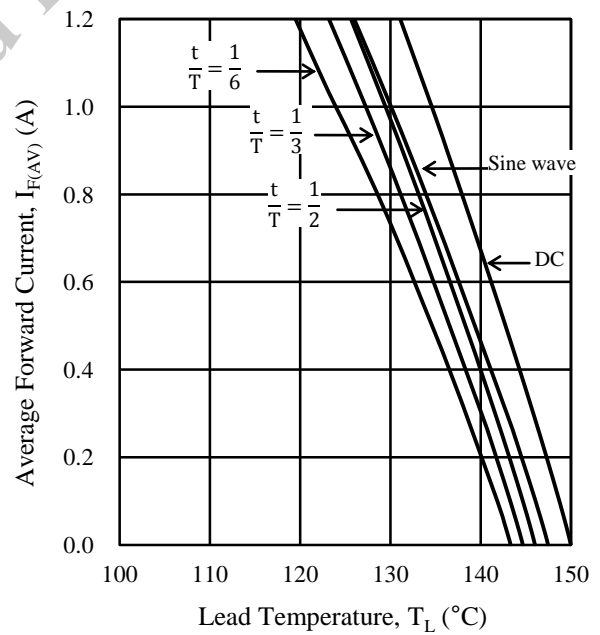


Figure 4. T_L vs. $I_{F(AV)}$ Derating Curves ($V_R = 800\text{ V}$, $T_J = 150\text{ }^\circ\text{C}$)

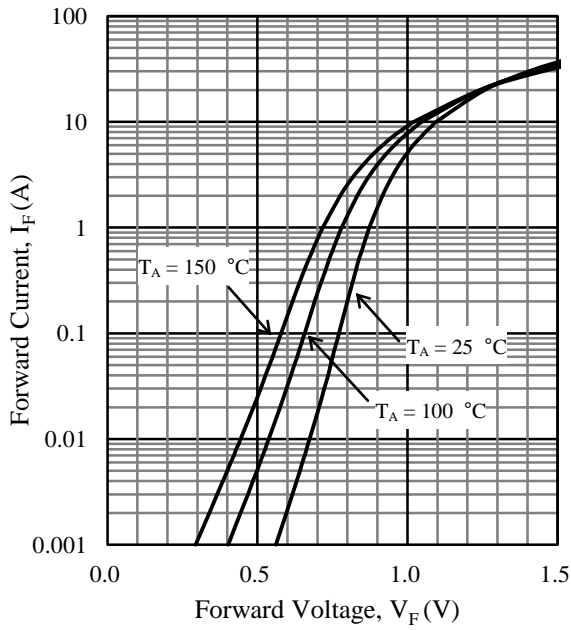


Figure 5. V_F vs. I_F Typical Characteristics

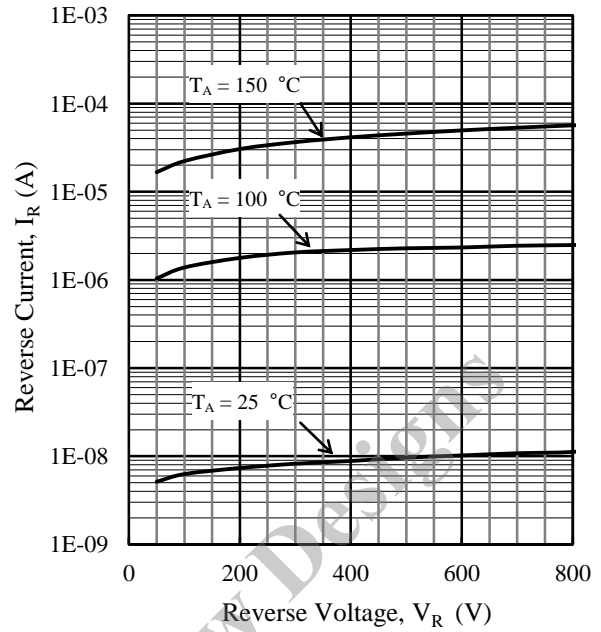


Figure 6. V_R vs. I_R Typical Characteristics

SARS02 Rating and Characteristic Curves

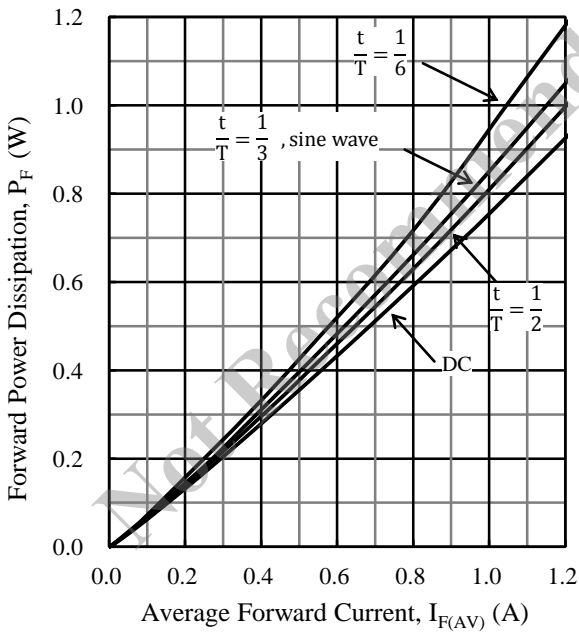


Figure 7. $I_{F(AV)}$ vs. P_F Power Dissipation Curves ($T_J = 150\text{ °C}$)

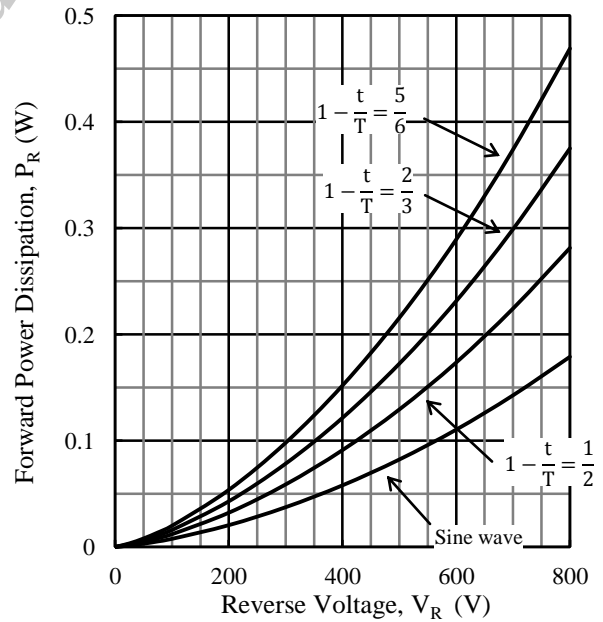


Figure 8. V_R vs. P_R Power Dissipation Curves ($T_J = 150\text{ °C}$)

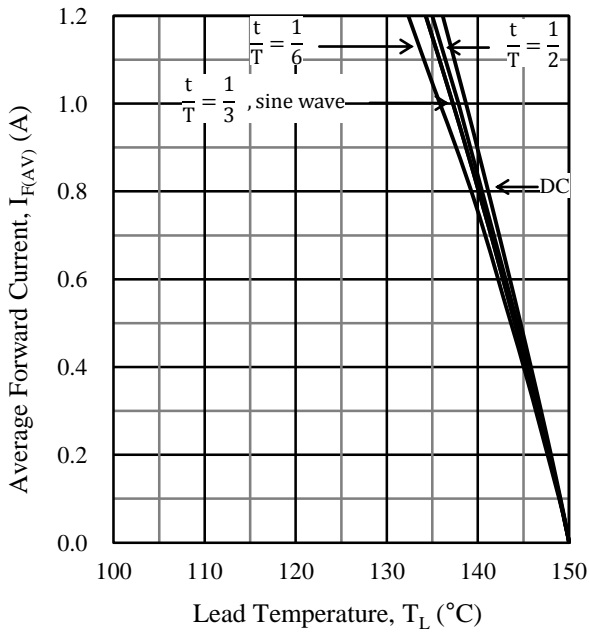


Figure 9. T_L vs. $I_{F(AV)}$ Derating Curves
($V_R = 0$ V, $T_J = 150$ °C)

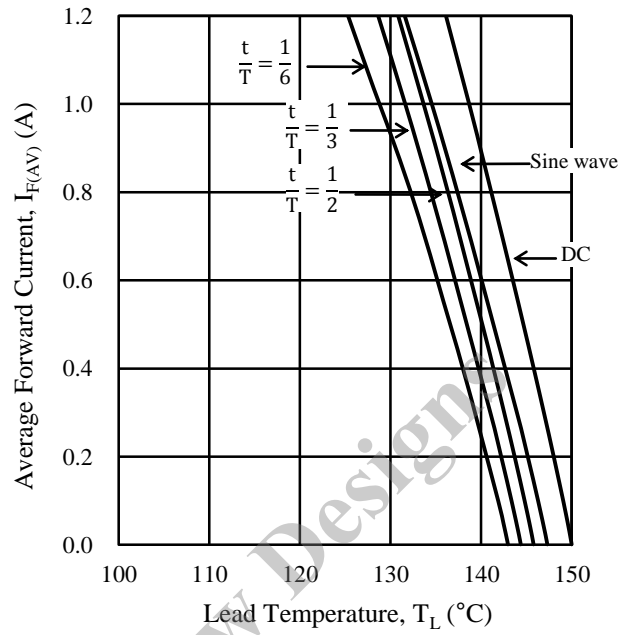


Figure 10. T_L vs. $I_{F(AV)}$ Derating Curves
($V_R = 800$ V, $T_J = 150$ °C)

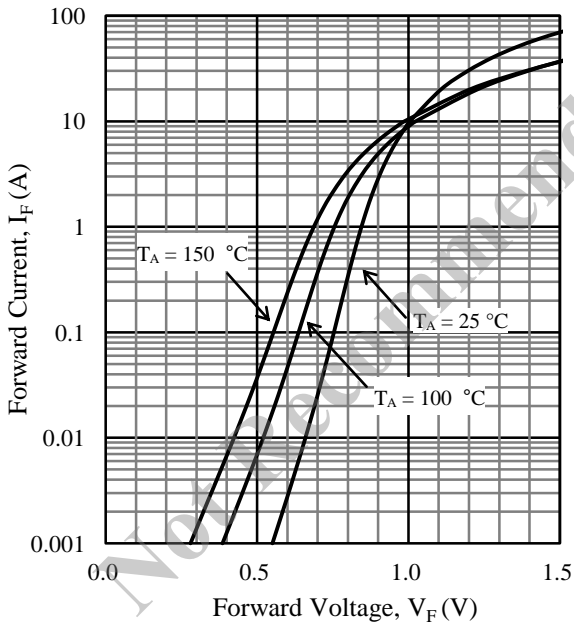


Figure 11. V_F vs. I_F Typical Characteristics

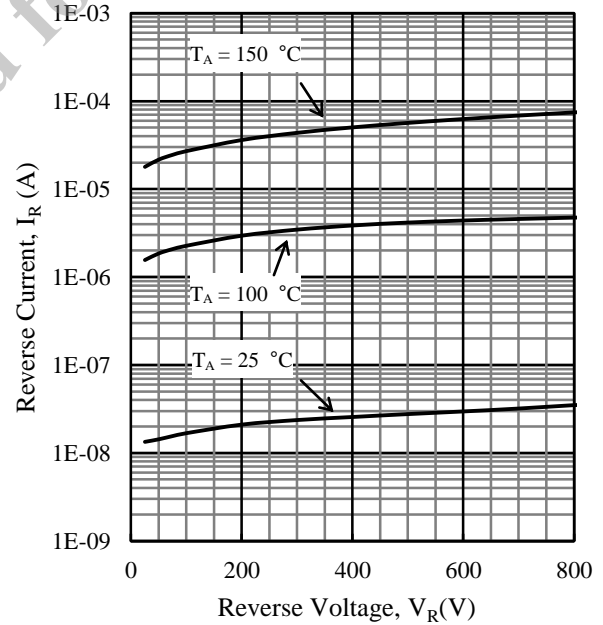


Figure 12. V_R vs. I_R Typical Characteristics

SARS05 Rating and Characteristic Curves

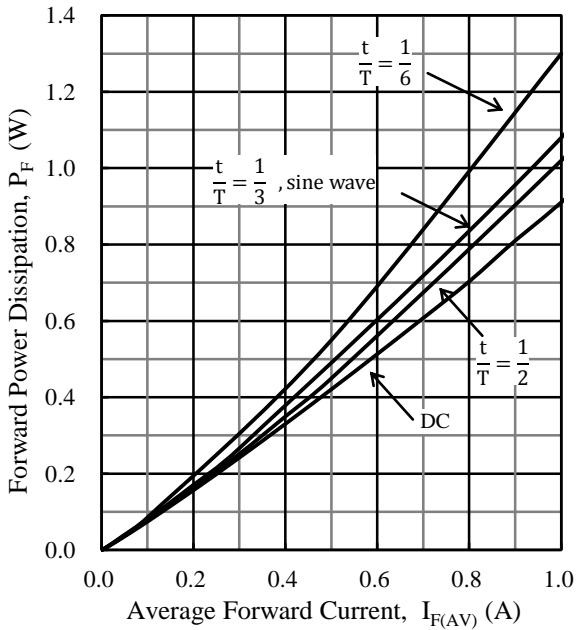


Figure 13. $I_{F(AV)}$ vs. P_F Power Dissipation Curves ($T_J = 150\text{ }^\circ\text{C}$)

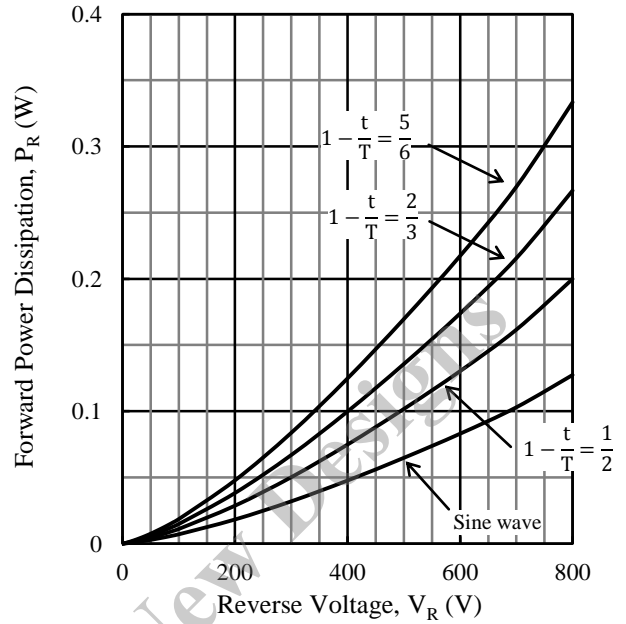


Figure 14. V_R vs. P_R Power Dissipation Curves ($T_J = 150\text{ }^\circ\text{C}$)

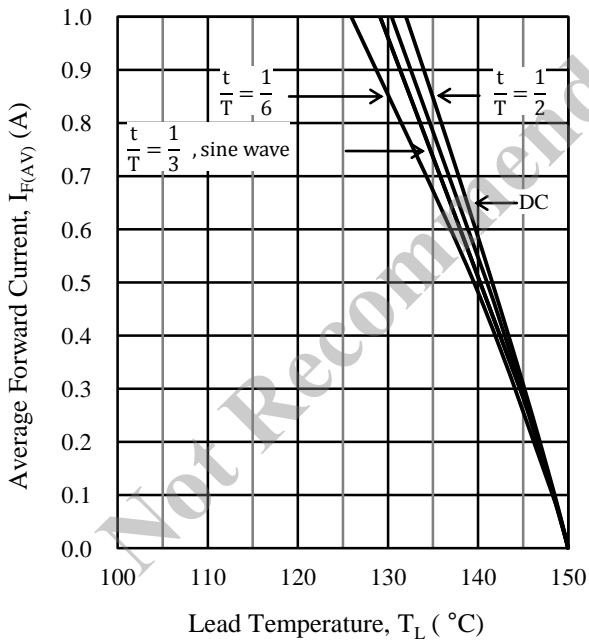


Figure 15. T_L vs. $I_{F(AV)}$ Derating Curves ($V_R = 0\text{ V}$, $T_J = 150\text{ }^\circ\text{C}$)

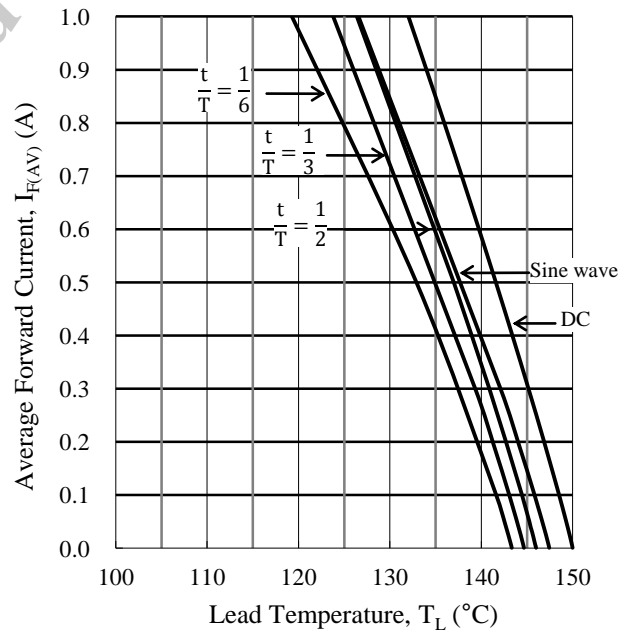


Figure 16. T_L vs. $I_{F(AV)}$ Derating Curves ($V_R = 800\text{ V}$, $T_J = 150\text{ }^\circ\text{C}$)

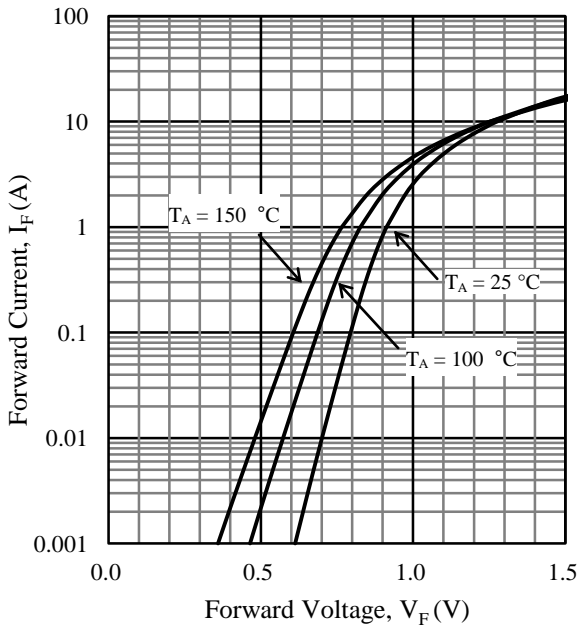


Figure 17. V_F vs. I_F Typical Characteristics

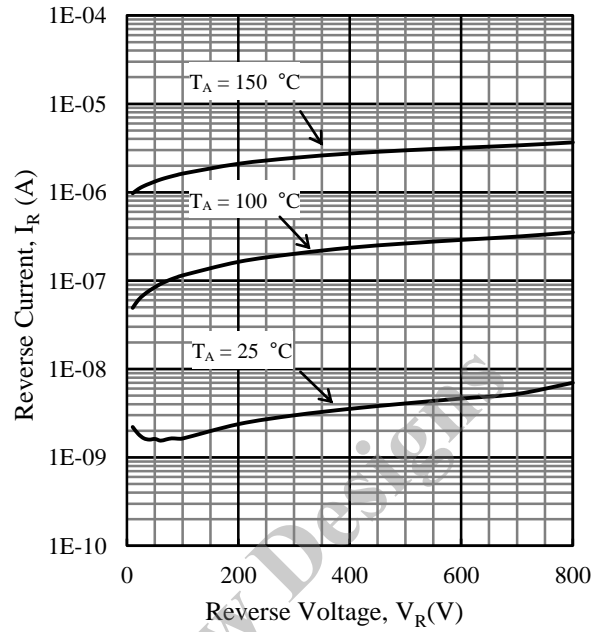


Figure 18. V_R vs. I_R Typical Characteristics

SARS10 Rating and Characteristic Curves

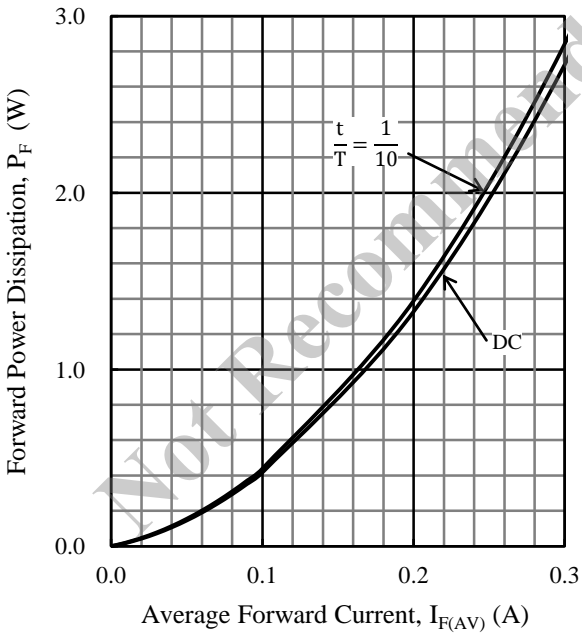


Figure 19. $I_{F(AV)}$ vs. P_F Power Dissipation Curves ($T_J = 125\text{ °C}$)

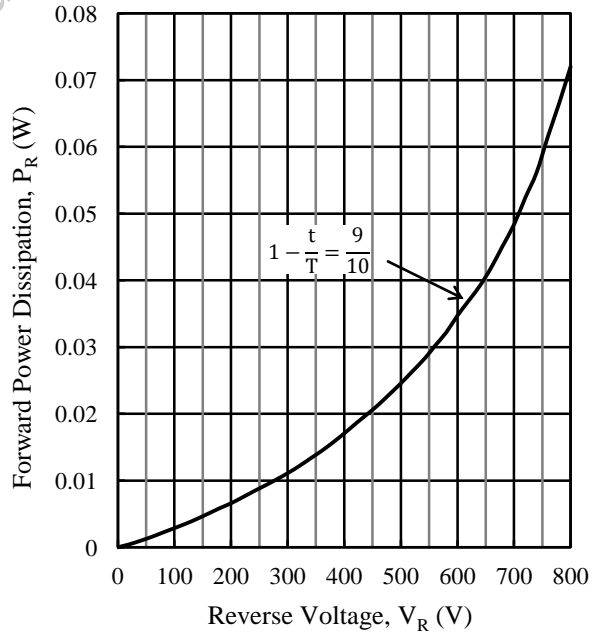


Figure 20. V_R vs. P_R Power Dissipation Curve ($T_J = 125\text{ °C}$)

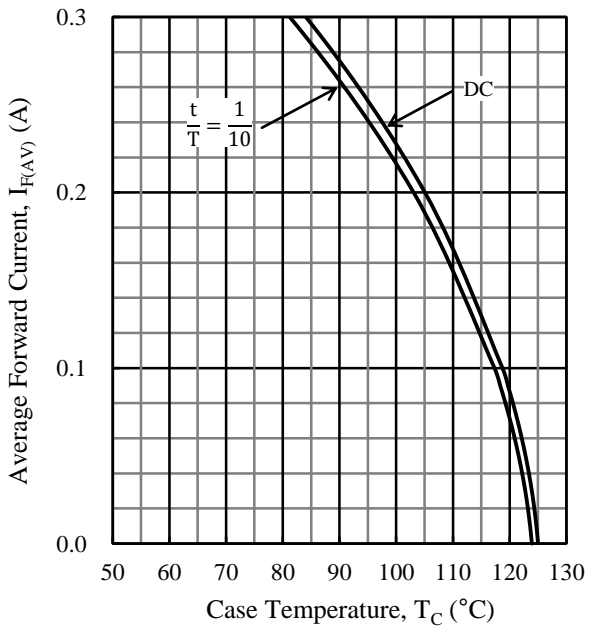


Figure 21. T_C vs. $I_{F(AV)}$ Derating Curves
($V_R = 800\text{ V}$, $T_J = 125\text{ }^\circ\text{C}$)

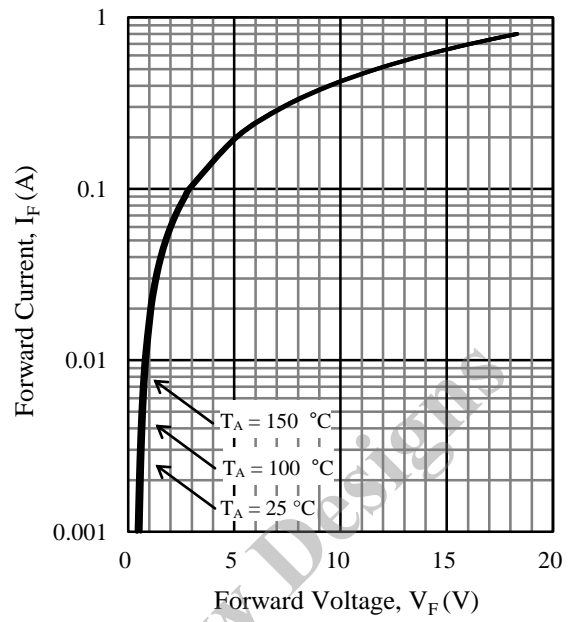


Figure 22. V_F vs. I_F Typical Characteristics

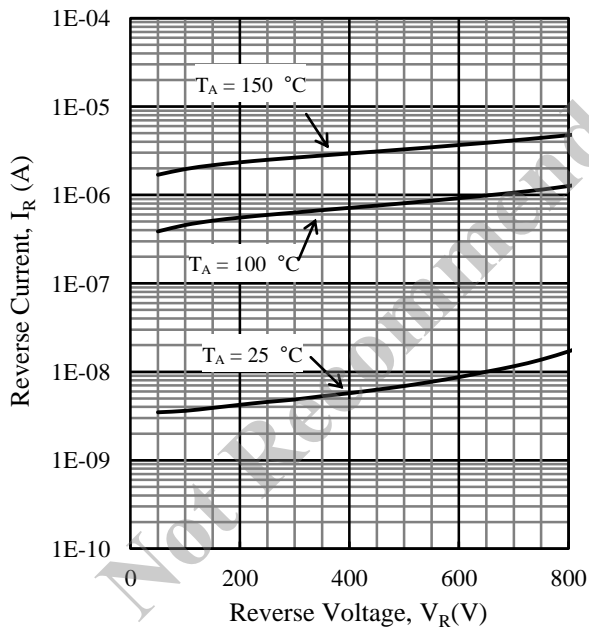


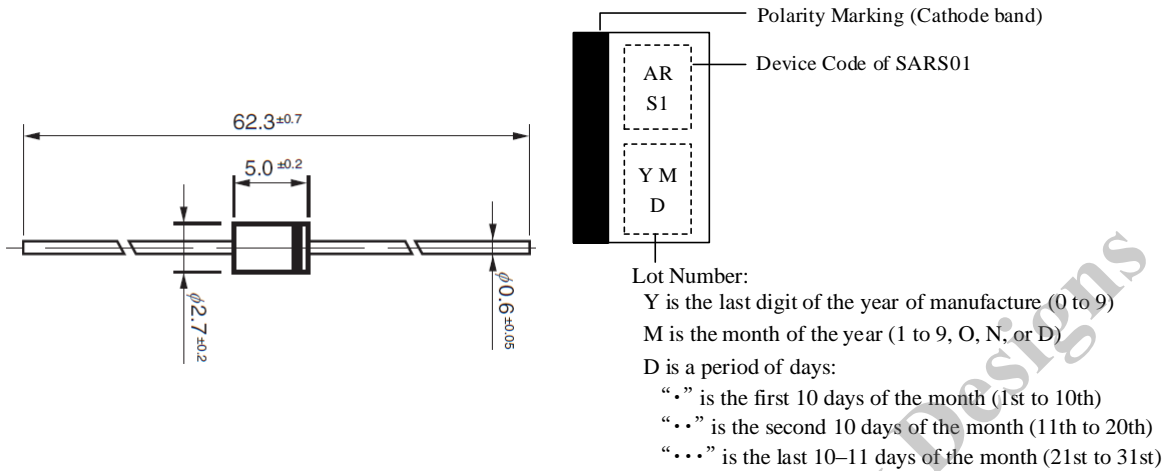
Figure 23. V_R vs. I_R Typical Characteristics

SARS01, SARS02, SARS05, SARS10

Physical Dimensions and Marking Diagrams

• SARS01

Axial (ϕ 2.7 / ϕ 0.6)

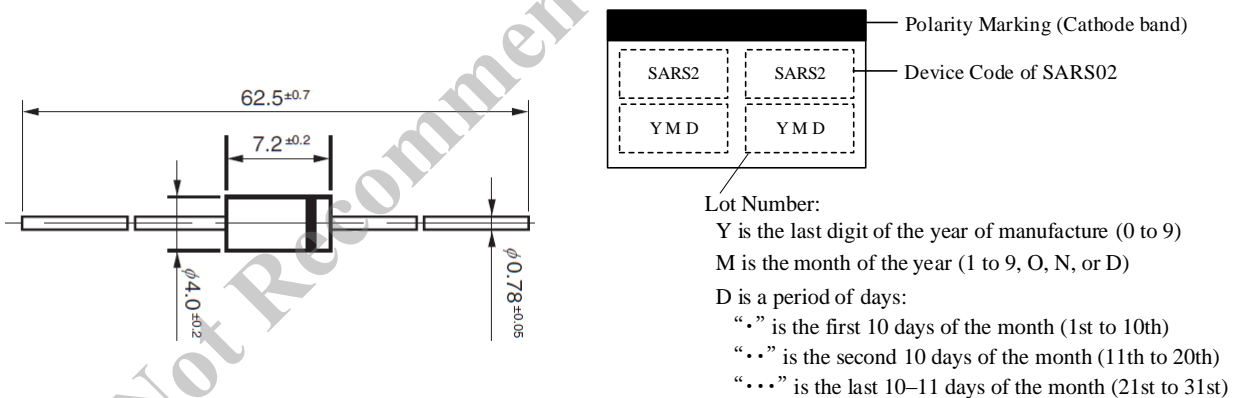


NOTES:

- Dimensions in millimeters
- Bare lead: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time, within the following limits:
 Flow: 260 ± 5 °C / 10 ± 1 s, 2 times
 Soldering Iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)

• SARS02

Axial (ϕ 4 / ϕ 0.78)



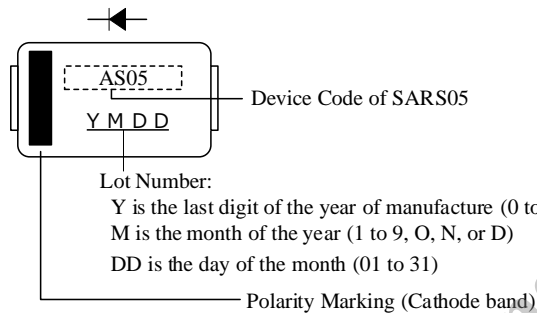
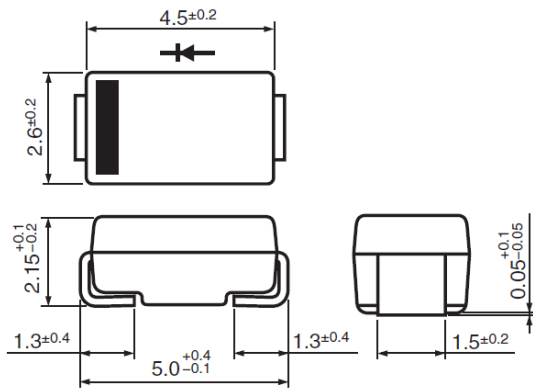
NOTES:

- Dimensions in millimeters
- Bare lead: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time within the following limits:
 Flow: 260 ± 5 °C / 10 ± 1 s, 2 times
 Soldering iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)

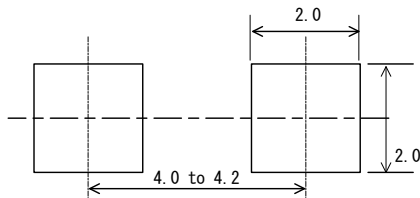
SARS01, SARS02, SARS05, SARS10

• SARS05

SJP 4.5 mm × 2.6 mm



SJP Land Pattern Example



NOTES:

- Dimensions in millimeters
- Bare lead frame: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time, within the following limits:

Reflow (MSL 1):

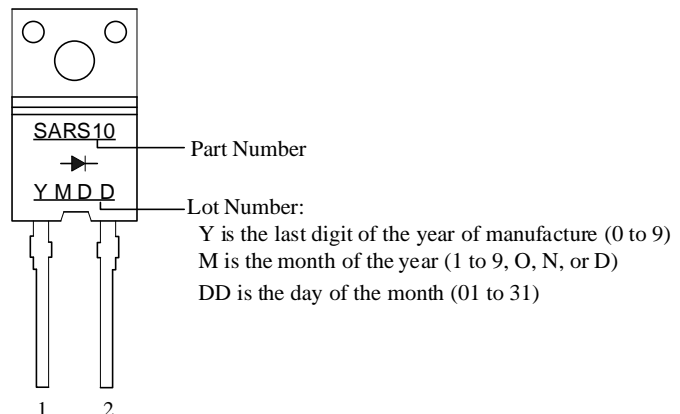
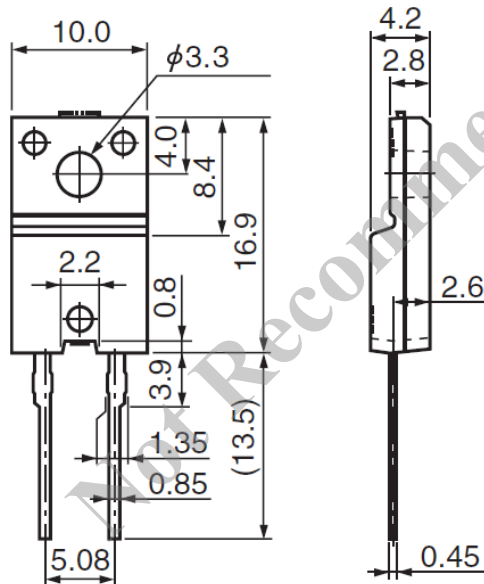
Preheat: 180 °C, 90 ± 30 s

Solder heating: 250 °C, 10 ± 1s, 2 times (260 °C peak)

Soldering iron: 380 ± 10 °C, 3.5 ± 0.5s, 1 time

• SARS10

TO220F-2L



NOTES:

- Dimensions in millimeters
- Bare lead frame: Pb-free (RoHS compliant)
- When soldering the products, be sure to minimize the working time, within the following limits:
 Flow: 260 ± 5 °C / 10 ± 1 s, 2 times
 Soldering Iron: 380 ± 10 °C / 3.5 ± 0.5 s, 1 time (Soldering should be at a distance of at least 1.5 mm from the body of the products.)
- The recommended screw torque for TO220F: 0.490 N·m to 0.686 N·m (5 kgf·cm to 7 kgf·cm)

Operational Comparison of Clamp Snubber Circuits

Figure 24 shows a general clamp snubber circuit. In the circuit, the surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop, and is consumed by R_{S1} through the energy discharge loop. All the consumed energy becomes loss in R_{S1} . In addition, the ringing of surge voltage results in poor cross regulation of multi-outputs.

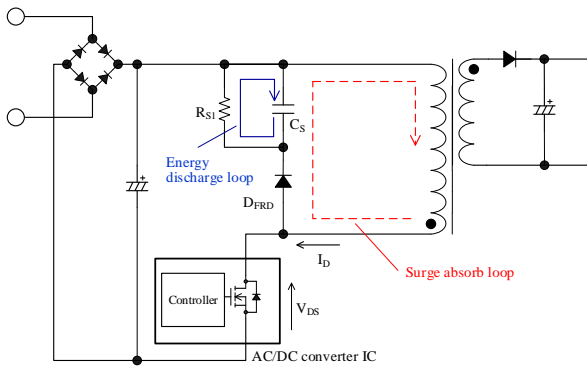


Figure 24. General Clamp Snubber Circuit

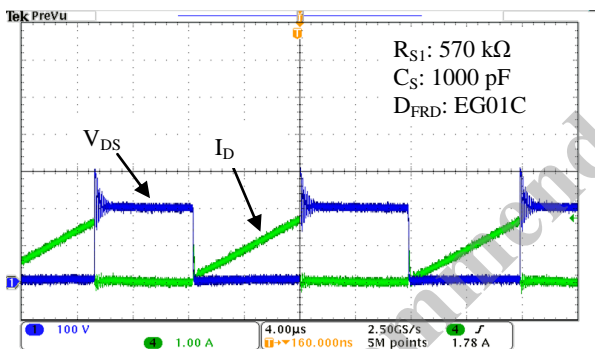


Figure 25. Waveforms of General Clamp Snubber Circuit

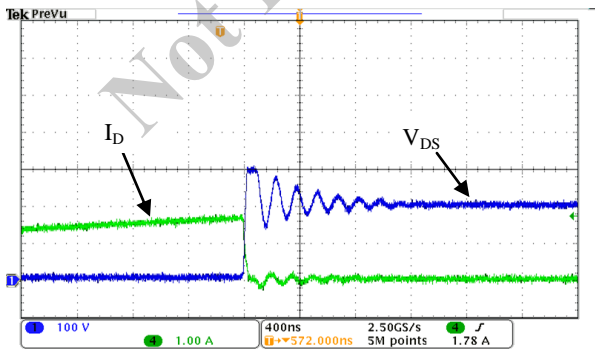


Figure 26. Enlarged View of Figure 25

Figure 27 shows the clamp snubber circuit using the SARS. The surge voltage at tuning off a power MOSFET is charged to C_S through the surge absorb loop. Since the reverse recovery time, t_{rr} , of the SARS is a relatively long period, the energy charged to C_S is discharged to the reverse direction of the surge absorb loop until C_S voltage is equal to the flyback voltage. Thus, the power supply efficiency improves.

In addition, the power supply using the SARS reduces the ringing voltage. Thus, the cross regulation of multi-outputs can be improved.

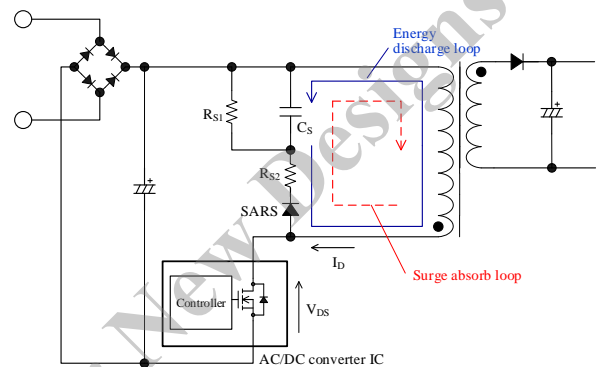


Figure 27. Clamp Snubber Circuit using SARS

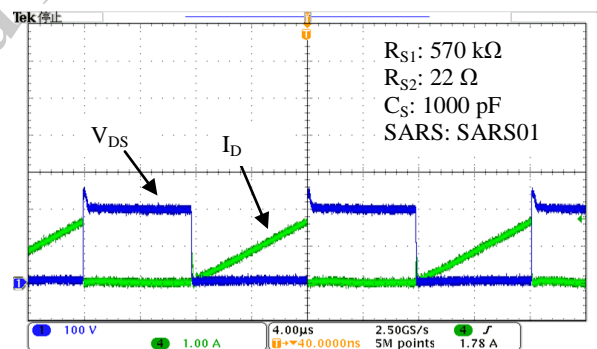


Figure 28. Waveforms of Clamp Snubber Circuit using SARS

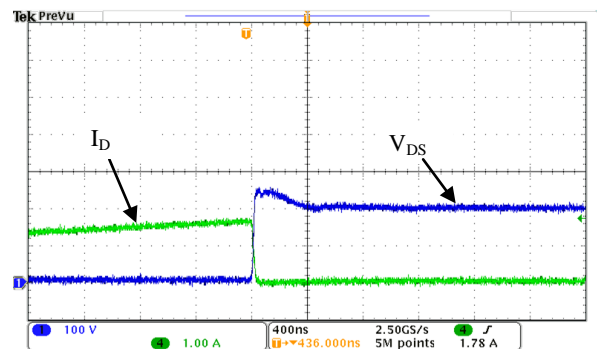


Figure 29. Enlarged View of Figure 28

Power Dissipation and Junction Temperature Calculation

Figure 30 shows a typical application using the SARS. Figure 31 shows the operating waveforms of the SARS.

The power dissipation of the SARS is calculated as follows:

- 1) The waveforms of the SARS voltage, V_{SARS} , and the SARS current, I_{SARS} , are measured in actual application operation. $V_{SARS} \times I_{SARS}$ is calculated by the math function of oscilloscope. (Since the SARS10 incorporates a resistor, $V_{SARS(10)}$ is measured.)
- 2) The each average energy ($P_1, P_2 \dots P_k$) is measured at period of each polarity of $V_{SARS} \times I_{SARS}$ ($t_1, t_2, \dots t_k$) as shown in Figure 30 by the automatic measurement function of the oscilloscope.
- 3) The power dissipation of the SARS, P_{SARS} , is calculated by Equation (1):

$$P_{SARS} = \frac{1}{T} (|P_1 \times t_1| + |P_2 \times t_2| + \dots |P_k \times t_k|) \quad (1)$$

where:

P_{SARS} is power dissipation of the SARS,
 T is switching cycle of power MOSFET (s), and
 P_k is average energy of period t_k (W).

A differential probe is recommended to use for the measurement of V_{SARS} . Please conform to the oscilloscope manual about power dissipation measurement including the delay compensation of probe.

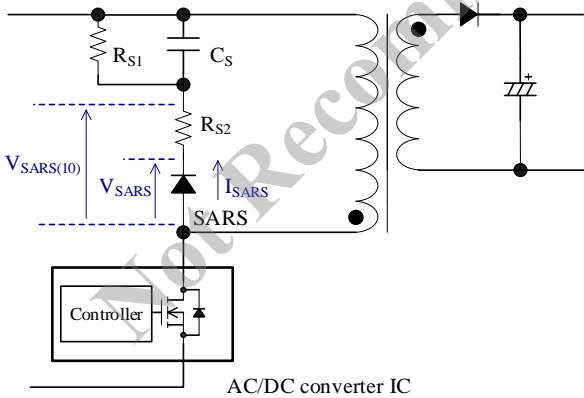


Figure 30. Typical Application

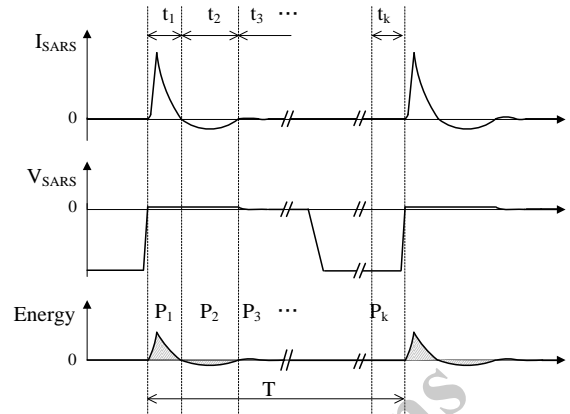


Figure 31. SARS Current

In addition, by using the temperature of the SARS in actual application operation, the estimated junction temperature of the SARS is calculated by Equation (2) and Equation (3). It should be enough lower than T_J of the absolute maximum rating.

• SARS01/02/05

$$T_{J(SARS)} = T_L + \theta_{J-L} \times P_{SARS} \text{ (}^\circ\text{C)} \quad (2)$$

where:

$T_{J(SARS)}$ is junction temperature of the SARS,
 T_L is lead temperature of the SARS, and
 θ_{J-L} is thermal resistance between junction to lead.

• SARS10

$$T_{J(SARS)} = T_C + \theta_{J-C} \times P_{SARS} \text{ (}^\circ\text{C)} \quad (3)$$

Where:

$T_{J(SARS)}$ is junction temperature of the SARS,
 T_C is case temperature of the SARS, and
 θ_{J-C} is thermal resistance between junction to case.

Parameter Setting of Snubber Circuit using SARS

The temperature of the SARS and peripheral components should be measured in actual application operation.

The reference values of snubber circuit using the SARS are as follows:

- **C_S**
680 pF to 0.01 μF.
The voltage rating is selected according to the voltage subtracted the input voltage from the peak of V_{DS}.

- **R_{S1}**
R_{S1} is the bias resistance to turn off the SARS, and is 100 kΩ to 1 MΩ.
Since a high voltage is applied to R_{S1} that has high resistance, the following should be considered according to the requirement of the application:
 - Select a resistor designed for electromigration, or
 - Connect more resistors in series so that the applied voltages of individual resistors can be reduced.The power rating of resistor should be selected from the measurement of the effective current of R_{S1} based on actual operation in the application.

- **R_{S2}**
R_{S2} is the limited resistance in the energy discharging. The value of 22 Ω to 220 Ω is connected to the SARS in series (the SARS10 incorporates R_{S2}).
The power rating of resistor should be selected from the measurement of the effective current of R_{S2} based on actual operation in the application.

Not Recommended for New Designs

SARS01, SARS02, SARS05, SARS10

• Transformer Specifications

Item	Specification
Primary Inductance, L_P	518 μ H
Core Size	EER-28
AL Value	245 nH/ N^2 (with a center gap of about 0.56 mm)
Winding Specification	See Table 1
Winding Structure	See Figure 32

Table 1. Winding Specification

Winding	Symbol	Number of Turns (turns)	Wire Diameter (mm)	Structure
Primary Winding	P1	18	ϕ 0.23 \times 2	Single-layer, solenoid winding
Primary Winding	P2	28	ϕ 0.30	Single-layer, solenoid winding
Auxiliary Winding	D	12	ϕ 0.30 \times 2	Solenoid winding
Output 1 Winding	S1-1	6	ϕ 0.4 \times 2	Solenoid winding
Output 1 Winding	S1-2	6	ϕ 0.4 \times 2	Solenoid winding
Output 2 Winding	S2-1	4	ϕ 0.4 \times 2	Solenoid winding
Output 2 Winding	S2-2	4	ϕ 0.4 \times 2	Solenoid winding

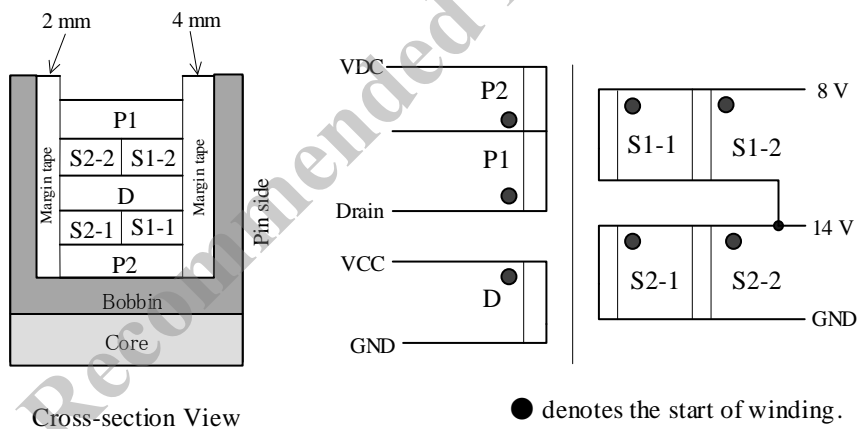


Figure 32. Winding Structure

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