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Keywords: zener references, bandgap, references, voltage reference selection

APPLICATION NOTE 2879

Selecting the Optimum Voltage Reference

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Abstract: What could be more basic than a voltage reference—a simple, constant reference voltage? As with all design topics, there are tradeoffs. This article discusses the different types of voltage references, their key specifications, and the design tradeoffs, including accuracy, temperature-independence, current drive capability, power dissipation, stability, noise, and cost.

You can find voltage references inside almost any advanced electronic product, either standalone or integrated into larger functions. Understanding the technology as well as the system error budget is an important design consideration. Because of limited space, we suggest further reading in the footnotes as we touch on system concepts. For example:

1. In a voltage regulator, a reference provides a known value that is compared to the output to develop the feedback used to regulate the output voltage¹.
 - a. Remote voltage adjustment and power-supply margining may be needed in the application^{2, 3, 4}.
2. In a data converter, a reference provides an absolute voltage to compare to the input voltage to determine the proper digital code⁵.
 - a. Error budgets for an analog-to-digital converter (ADC) and a voltage reference; or digital-to-analog converter (DAC) and a voltage reference combination⁶.
 - b. Other data converter error sources, effective resolution, and number of bits^{7, 8}.
 - c. Tools and calculators for converter accuracy and clock jitter, signal bandwidth, and THD^{9, 10}.
3. In a voltage detector circuit, the reference is used as an absolute threshold to set the trip point¹¹.

The required specifications depend on the application. This article discusses the different types of voltage references, their key specifications, and design tradeoffs. It offers information to help designers select the optimum voltage reference for their applications.

The Ideal

An ideal voltage reference has a perfect initial accuracy and maintains its voltage independent of changes in load current, temperature, and time. In the real world, a designer must make tradeoffs such as: initial

voltage accuracy, voltage temperature drift and hysteresis, current source and sink capability, quiescent current (or power dissipation), long-term stability, noise, and cost.

Types of Reference

The two most common types of references are zener and bandgap^{12, 13}. Zeners are usually used in two-terminal shunt topologies. Bandgap references are usually used in three-terminal series topologies.

Zener Diodes and Shunt Topologies

Zener diodes are diodes optimized for operation in the reverse-bias breakdown region. Because breakdown is relatively constant, it can be used to generate a stable reference by driving a known current in the reverse direction.

One big advantage of zeners is the wide range of voltages that are available, from 2V up to 200V. They also have a wide range of power handling capability, from several milliwatts to several watts.

The key disadvantages of zener diodes is that they are not precise enough for high-precision applications and their power consumption makes them a tough fit for low-power applications. An example is the BZX84C2V7LT1G, which has a breakdown, or nominal reference voltage, of 2.5V with a variation from 2.3V to 2.7V, or $\pm 8\%$ accuracy. This is suitable only for applications that need little precision.

An additional concern with a zener reference is the output impedance. Our example above has an internal impedance of 100Ω at 5mA and 600Ω at 1mA. A non-zero impedance causes an additional variation in the reference voltage depending on the variation in load current. Selecting a zener with low output impedance minimizes this effect.

Buried zener diodes are a specific type of zener that are more stable than a regular zener, due to their structure, which places them below the surface of the silicon.

An alternative to an actual zener diode is an active circuit that emulates a zener. Circuitry allows the device to significantly improve upon the classic limitations of the zener. One such device is the [MAX6330](#). It has a tight 1.5% (max) initial accuracy over a $100\mu\text{A}$ to 50mA variation in load. A typical implementation of this type of IC is shown in **Figure 1**.

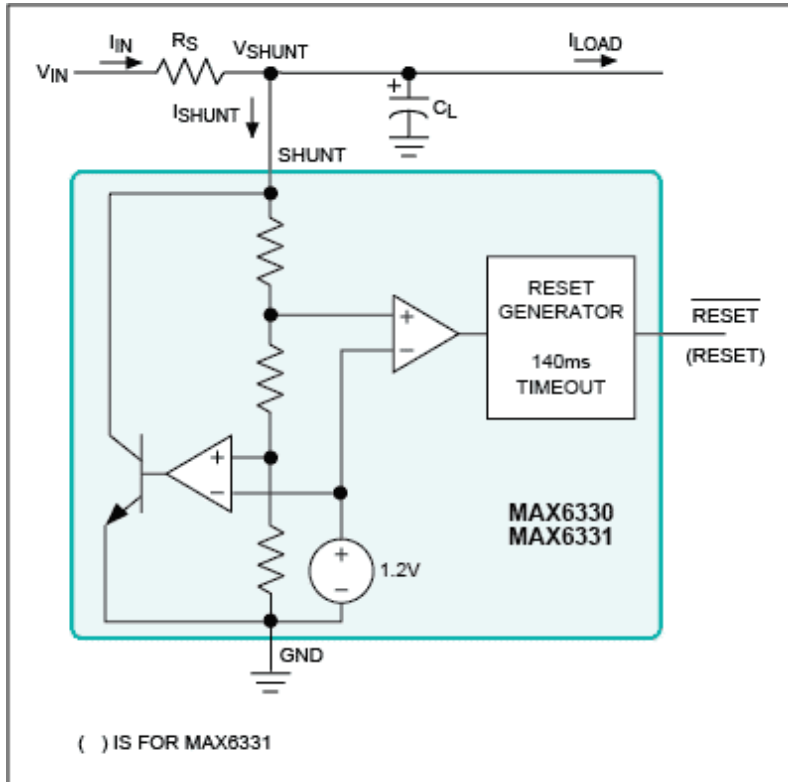


Figure 1. Using the MAX6330 as an active circuit that emulates a zener diode.

Selecting the Proper Shunt Resistor

All shunt configuration references need a current-limiting resistor in series with the reference element. It can be calculated from the following equation:

$$R_S = (V_{IN(max)} - V_{SHUNT(min)}) / (I_{SHUNT(max)} + I_{LOAD(min)}) \leq R_S \leq (V_{IN(min)} - V_{SHUNT(max)}) / (I_{SHUNT(min)} + I_{LOAD(max)})$$

where:

V_{IN} is the input voltage range

V_{SHUNT} is the regulated voltage

I_{LOAD} is the output current range

I_{SHUNT} is the minimum shunt operating current

Note that a shunt circuit *always* consumes $I_{LOAD(max)} + I_{SHUNT}$ whether or not a load is present.

The same shunt can be used for $10V_{IN}$ or $100V_{IN}$ by properly sizing R_S . Choosing the largest nominal resistor value for R_S gives the lowest current consumption. Remember to provide a safety margin to incorporate the worst-case tolerance of the resistor used. You should also ensure that the resistor's power rating is adequate, using either of the following two general power equations:

$$\begin{aligned}
 P_R &= I_{IN}(V_{IN(max)} - V_{SHUNT}) \\
 &= I_{IN}^2 R_S \\
 &= (V_{IN(max)} - V_{SHUNT})^2 / R_S
 \end{aligned}$$

Bandgap References and Series Mode Topologies

The key differences between a shunt and series reference is that the three terminal series-mode voltage references do not require an external resistor and have significantly lower quiescent power. The most common form is the ubiquitous bandgap reference.

Bandgap Basics

A bandgap reference develops two voltages: One has a positive temperature coefficient (tempco) and one has a negative tempco. Together, they have a zero-tempco sum at the output.

The positive tempco is usually derived from the difference of two V_{BE} 's running at different current levels. The negative tempco uses the naturally negative tempco of the V_{BE} voltage (see **Figure 2**).

In practice, the tempco sum is not exactly zero. Depending on design details like the IC circuit design, packaging, and manufacturing test capabilities, these devices can usually achieve a V_{OUT} tempco between 1 and 100ppm per degree C.

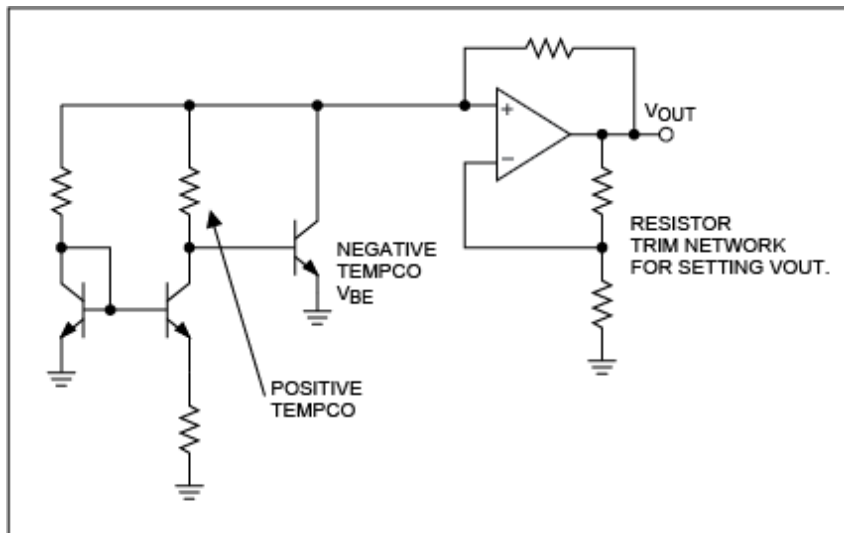


Figure 2. Bandgap voltage reference.

Maxim's Bandgap Reference Calculator (BGRC) Users Guide (in the Calculator zip file) allows one to simulate a Brokaw Bandgap reference cell. The effect of trimming the bandgap is shown for temperatures from absolute zero to 175°C. The curvature correction circuit is also adjustable to allow a design engineer to understand the reference IC design process. The physics behind the design becomes apparent along with an understanding of the resulting error waveforms and magnitude.

The use of either a shunt or series topology is typically dictated by the application and the desired performance. See **Table 1** for some comparisons between zeners in shunt topologies and bandgaps in

series topologies.

What	Zener - Shunt Topology	Buried Zener - Shunt Topology	Bandgap - Series Topology
Pros	<ul style="list-style-type: none"> • Wide/high V_{IN} capable • Best for non-power-critical applications due to higher $I_{QUIESCENT}$ (1mA to 10mA) • > 1% FS initial accuracy 	<ul style="list-style-type: none"> • Wide/high V_{IN} capable • Best for non-power-critical applications due to higher $I_{QUIESCENT}$ (1mA to 10mA) • 0.01% to 0.1% FS initial accuracy 	<ul style="list-style-type: none"> • Typically lower V_{IN} range • Low quiescent current (μA to $\sim 1mA$) • No external resistor • Lower $I_{QUIESCENT}$ • 0.05% to 1% FS initial accuracy • Low dropout voltages
Cons	<ul style="list-style-type: none"> • Current is always used • Requires external resistor • Lower precision • Can only sink current • High dropout voltage 	<ul style="list-style-type: none"> • Higher $I_{QUIESCENT}$ than bandgaps 	<ul style="list-style-type: none"> • Limited V_{IN} range • Pass element losses
Gotchas	<ul style="list-style-type: none"> • Long-term stability 	<ul style="list-style-type: none"> • Not all series devices sink current 	<ul style="list-style-type: none"> • Not all series devices sink current

System Design Issues and Reference Selection

Power Consumption

If you are designing a medium precision system like a high-efficiency, $\pm 5\%$ power supply or perhaps an 8-bit data acquisition system that requires minimal power, you could use a device like the [MAX6025](#) or [MAX6192](#). Both are 2.5V references that consume a maximum of $35\mu A$. They have very low output impedance so the reference voltage is virtually independent of I_{OUT} .

Source and Sink Current

Another specification is the reference's ability to source and sink current.

Most applications require a voltage reference to source current to the load(s) and, of course, the reference needs to be able to supply the required load current. It also needs to supply any I_{BIAS} or leakage currents—their sum can sometimes exceed the load currents.

ADCs and DACs typically require between tens of micro-amps for a converter like the [MAX1110](#), to 10mA (max) for devices like the AD7886. The [MAX6101–MAX6105](#) family of references sources 5mA and sinks 2mA. For really heavy loads, the [MAX6225/MAX6241/MAX6250](#) family sources and sinks 15mA.

Temperature Drift

Temperature drift is normally a correctable parameter^{14, 15}. It is typically a very repeatable error. Correction can be accomplished by adding a calibration step or by reading a value from a look-up function that has been previously characterized.

Output Voltage Temperature Hysteresis

This parameter is defined as the change in output voltage at the reference temperature (+25°C) due to sequential but opposite temperature excursions (i.e. hot-to-cold and then cold-to-hot). Very negative effects can occur due to this effect since its amplitude is directly proportional to the temperature excursion the system underwent. In many systems this type of error is not very repeatable. This parameter is a function of design of the IC circuit as well as effects from the packaging. For example: The MAX6001 device in a 3-pin SOT23 has a typical temperature hysteresis of 130ppm. But a larger, more stable package, like the MAX6190 in the 8-pin SO, has only 75ppm.

Calibration^{16, 17, 18, 19, 20}

Calibration is very common in high-resolution systems. In a 16-bit system, you need better than a 1ppm/°C reference for the commercial (0°C to +70°C) temperature range to stay within the ± 1 LSB over the entire range, with a +25°C reference point. $\Delta V = (1\text{ppm}/^\circ\text{C} \times 5\text{V} \times 45^\circ\text{C}) = 255\mu\text{V}$. This same temperature drift extended over the industrial temperature range is only acceptable for a 14-bit system.

- Why one should calibrate, correcting component tolerance, gain, and offset^{16, 17}.
- Free calculators for ADC and DAC accuracy and thermal noise^{19, 20}.
- Design tools of simulation, decoupling capacitors, and filters (free or low cost)¹⁸.
- Calibration circuit ideas, tips, and FAQs^{21, 22, 23, 24}.

Noise

Noise usually consists of random thermal noise, but can also include flicker noise and other spurious sources. The [MAX6150](#), MAX6250, and [MAX6350](#) are all good choices for low noise applications with 35 μV , 3 μV , and 3 μV_{P-P} noise performance, respectively. All of these contribute less than 1 LSB of noise into your measurement. One could over-sample and average, but it comes at the cost of processor power and increased system complexity and cost.

Maxim's Thermal Noise Calculator (TNC) Users Guide (in the Calculator zip file) aids in the analysis of thermal noise found in resistors and other noise sources. TNC finds the noise voltage generated by any device if its white-noise spectral density and 1/f corner frequency are known. TNC can also be run on a

HP 50g calculator or a PC using a free emulator program.

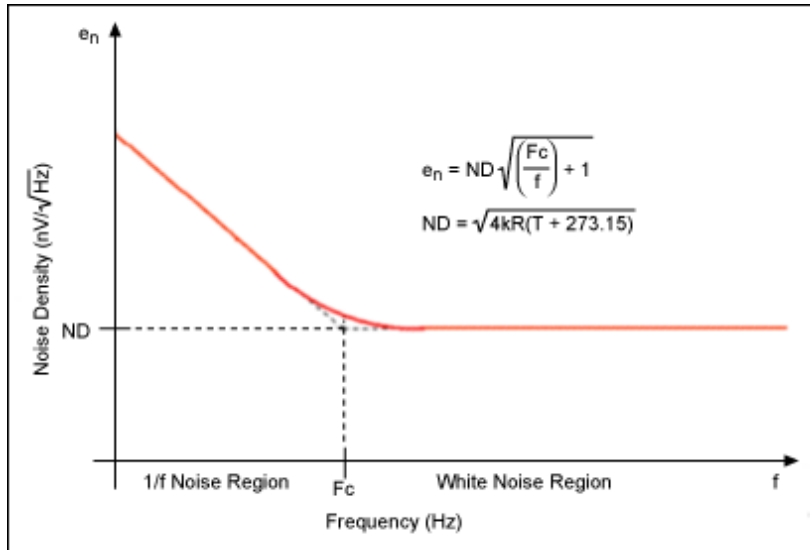


Figure 3. Typical spectral noise density.

The thermal noise calculator can show the noise contribution for a customer over a specified bandwidth.

Long-Term Stability

This parameter is defined as a change in voltage over time. It is primarily due to die stress or perhaps ion migration that exists in a package or family of devices. It is important to note that the circuit board cleanliness can show up as a long-term change over time; especially over temperature and humidity. This effect, at times can be larger than the inherent device stability. Long-term stability is typically only specified at the reference temperature, usually $+25^\circ\text{C}$.

Summary

The difficulties of designing any system lie in balancing the tradeoffs: cost, size, precision, power consumption, etc. It is important to consider all of the pertinent parameters when selecting the optimum reference for a design. It is interesting to note that many times a more expensive component can result in a lower total system cost due to the reduction in cost of compensation/calibration in manufacturing phase.

References

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2. Application note 4936, "[Calibrating a Power Supply with a Digital Potentiometer](#)"
3. Tutorial 5067, "[Margining and Calibration for Fun and Profit](#)"
4. Application note 226, "[Step-Up DC-DC Converter Calibration and Adjustment Using a Digital Potentiometer](#)"
5. Micro-Electronic Circuits, by Adel S. Sedra & Kenneth C. Smith, Chapter 3.6 *Operation in the Reverse Breakdown Region—Zener Diodes*, Chapter 10.9 to 10.11 *Data Converters*

6. Tutorial 4300, "Calculating the Error Budget in Precision Digital-to-Analog Converter (DAC)"
7. Tutorial 5353, "Calculating Effective Resolution for Data Converters"
8. Tutorial 4602, "Adjusting the Calibrating Out Offset and Gain Error in a Precision DAC"
9. Tutorial 5060, "ADC/DAC Accuracy Calculator Tutorial"
10. Tutorial 5061, "Effective Number of Bits Calculator Tutorial"
11. Tutorial 886, "Selecting the Right Comparator"
12. Tutorial 719, "Understanding Voltage-Reference Topologies and Specifications"
13. Application note 4003, "Series or Shunt Voltage Reference?"
14. Application note 4419, "Understanding Voltage-Reference Temperature Drift"
15. Application note 4672, "Understanding Temperature Drift in a Precision Digital-to-Analog Converter (DAC)"
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17. Application note 4494, "Methods for Calibrating Gain Error in Data-Converter Systems"
18. www.maximintegrated.com/cal
19. Tutorial 5275, "Calibration—Needless or a Necessity?"
20. Tutorial 5066, "When Is Calibration Important?"
21. Application note 4711, "Digital Calibration Makes Automated Test Easy; Calibration FAQs"
22. Tutorial 5036, "Calibration Circuit Library"
23. Application note 1956, "Tips to Remember When Designing with Digital Potentiometers"
24. Application note 593, "Digital Potentiometers: Frequently Asked Questions"

Related Parts

MAX6001	Low-Cost, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6002	Low-Cost, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6003	Low-Cost, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6004	Low-Cost, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6005	Low-Cost, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6012	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6021	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6025	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6030	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples

MAX6041	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6045	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6050	Precision, Low-Power, Low-Dropout, SOT23-3 Voltage References	Free Samples
MAX6120	Low-Cost, Micropower, Precision 3-Terminal, 1.2V Voltage Reference	Free Samples
MAX6125	SOT23, Low-Cost, Low-Dropout, 3-Terminal Voltage References	Free Samples
MAX6141	SOT23, Low-Cost, Low-Dropout, 3-Terminal Voltage References	Free Samples
MAX6145	SOT23, Low-Cost, Low-Dropout, 3-Terminal Voltage References	Free Samples
MAX6150	SOT23, Low-Cost, Low-Dropout, 3-Terminal Voltage References	Free Samples
MAX6160	SOT23, Low-Cost, Low-Dropout, 3-Terminal Voltage References	Free Samples
MAX6190	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6191	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6192	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6193	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6194	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6195	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6198	Precision, Micropower, Low-Dropout Voltage References	Free Samples
MAX6225	Low-Noise, Precision, +2.5V/+4.096V/+5V Voltage References	Free Samples
MAX6241	Low-Noise, Precision, +2.5V/+4.096V/+5V Voltage References	Free Samples
MAX6250	Low-Noise, Precision, +2.5V/+4.096V/+5V Voltage References	Free Samples
MAX6325	1ppm/°C, Low-Noise, +2.5V/+4.096V/+5V Voltage References	Free Samples
MAX6341	1ppm/°C, Low-Noise, +2.5V/+4.096V/+5V Voltage References	Free Samples
MAX6350	1ppm/°C, Low-Noise, +2.5V/+4.096V/+5V Voltage	Free Samples

References

MAX6520	50ppm/°C, SOT23, 3-Terminal, 1.2V Voltage Reference	Free Samples
MAX675	Precision, 5V Voltage Reference, Replaced MAX673	Free Samples
MAX872	10µA, Low-Dropout, Precision Voltage Reference	
MAX873	Low-Power, Low-Drift, +2.5V/+5V/+10V Precision Voltage Reference	Free Samples
MAX874	10µA, Low-Dropout, Precision Voltage Reference	
MAX875	Low-Power, Low-Drift, +2.5V/+5V/+10V Precision Voltage Reference	Free Samples
REF02	+5V, +10V Precision Voltage References	Free Samples

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